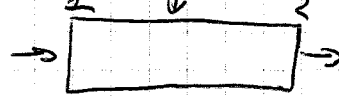


M<sub>10</sub> con addezione di NO<sub>2</sub>

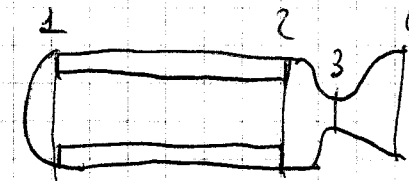


$\delta = 1.4, R = 287, P_0 = 1000 \text{ kPa}, T_0 = 500 \text{ K}, M_1 = 0.15, G_2/G_1 = 1.6$

$M_1 = 0.15 \xrightarrow{ISO} P_1/P_0 = 0.957, T_1/T_0 = 0.988 \rightarrow P_1 = 9.57 \cdot 10^5 \text{ Pa}, T_1 = 493.8 \text{ K}$   
 $\xrightarrow{M_1} \frac{P_1}{P^*} = 1.185, \frac{P_1}{P^*} = 2.207, \frac{P_1}{P^*} = 1.218, \frac{G_1}{G^*} = 0.8668$

$\frac{G_2}{G^*} = \frac{G_2}{G_1} \frac{G_1}{G^*} = 0.8108 \xrightarrow{M_2} M_2 = 0.647, \frac{T_2}{T^*} = \frac{P_2/P^*}{P_1/P^*} = \frac{P_2/P_1}{P^*/P_1}$   
 $\left. \begin{matrix} T_2 = 478 \\ P_2 = ? \end{matrix} \right\}$

$M_1 = 0.5, G_2/G_1 = 0.86$  come sopra



$D_1 = 0.075 \text{ m}, \dot{V} = 0.025 \text{ m}^3/\text{s}, \rho_1 = 2500 \text{ kg/m}^3$

$L_{12} = 0.30 \text{ m}, R = 320 \text{ J/kgK}, \delta = 1.4$

$T_{\text{Fiamma}} = 3000 \text{ K}, \dot{m} = ?, P_2 = ?, P_1 = ?, G^*$   
 $A_3 = 3.00 \cdot 10^{-4} \text{ m}^2$

$\dot{m} = \dot{V} \rho_1 \pi D_1 L = 1.473 \text{ kg/s}$   
 $A_1 = \pi D_1^2 / 4 = 4.909 \cdot 10^{-4} \text{ m}^2$

$\frac{P_2}{P^*} = 0.402, \frac{P_2}{P^*} = 0.386 \rightarrow M_2 = 0.386$

$\frac{P_2}{P^*} = 1.16, \frac{G_2}{G^*} = 0.7105$   
 S. superiore de  $T_{\text{Fiamma}} = T_0 \text{ sensore}$

$Q_0 = \sqrt{\delta R T_0} = 1159 \text{ m/s}$

$P_0 = \frac{\dot{m} Q_0}{A_3 \gamma^*} = 7024 \text{ kPa}$

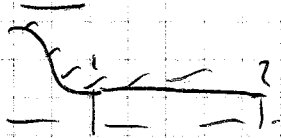
$M_1 = 0 \rightarrow \frac{P_0}{P^*} = 1.268$

$P_0 = \frac{P_0}{P^*} \frac{P^*}{P_2} P_2 = 7661 \text{ kPa}$

$G_2 = \frac{\dot{m}}{A_2} = 3000 \frac{\text{kg}}{\text{s}} \frac{1}{\pi \cdot 0.02^2} \Rightarrow G^* = 6023 \frac{\text{kg}}{\text{s m}^2}$

$P_2 = \frac{P_0}{P^*} P_2 = 6337 \text{ kPa}$

$\Delta P = P_2 - P_1 = P_2 - P_1 = 1326 \text{ kPa}$



$\delta = 1.4, R = 287, P_0 = 125 \text{ kPa}, T_0 = 350 \text{ K}, P_a = 100 \text{ kPa}, G_2/G_1 = 1.6$

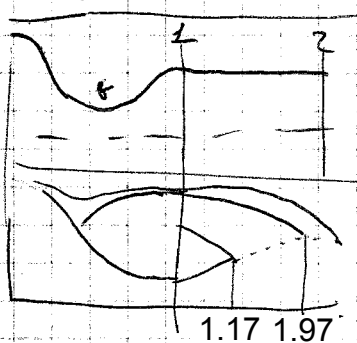
$M_1 = 1 \rightarrow \frac{G_1}{G^*} = 1, \frac{P_1}{P^*} = 1$

$\frac{G_1}{G^*} = \frac{G_1}{G_2} \frac{G_2}{G^*} = 0.625$

$M_1 = 0.324 \rightarrow \frac{P_1}{P^*} = 0.9300, \frac{P_1}{P^*} = 2.093$

$P_2 = \frac{P_0}{P^*} \frac{P^*}{P_1} P_1 = 55.54 \text{ kPa}$

Vedi Tabella E10.2



$\delta = 1.4, R = 287, P_0 = 600 \text{ kPa}, T_0 = 350 \text{ K}, A_1/A_0 = 2.4$

$A_1/A_0 \rightarrow M_1 = 2.60 \rightarrow \frac{G_1}{G^*} = 0.851 = 1/1.17, \frac{P_1}{P^*} = 0.0685, \frac{P_1}{P^*} = 0.265, \frac{P_1}{P^*} = 103.65, \frac{P_1}{P^*} = 0.259$

$M_1 = 0.250, \frac{P_1}{P^*} = 0.957, \frac{P_1}{P^*} = 173.35$

$\frac{G_1}{G^*} = 1/1.97, \frac{P_1}{P^*} = 2.206, \frac{P_1}{P^*} = 0.4339$

$P_0 = 350, G_2/G_1 = 1.5$  Velocità de  $P_2$  de n'he pannello peti

$\frac{G_2}{G^*} = \frac{G_2}{G_1} \frac{G_1}{G^*} = 0.761 \rightarrow M_2 = 0.624 \rightarrow P_2 = 331.142 < P_0$

$\frac{P_2}{P^*} = 1.408$  Tant'alt' come sopra

$P_0 = 180 \text{ kPa}$

Velocità  $P_2$

zuffocante

$M_2 = 1$

$\frac{G_1}{G^*} = \frac{1}{1.5} = 0.666 \rightarrow M_1 = 0.333 \rightarrow \frac{P_1}{P^*} = 2.044, \frac{P_1}{P^*} = 0.4174, \frac{A_1}{A^*} = 1.765$

$\frac{P_0}{P^*} = \frac{A^*}{A_1} = \frac{A}{A^*} \frac{A^*}{A_1} = 0.7334$

$P_2 = \frac{P_0}{P^*} \frac{P^*}{P_1} \frac{P_1}{P_2} P_2 = 132.1 < P_0 \rightarrow \text{ONDA D'URTO}$

$$M_2 = 0.6 \xrightarrow{M_1} G_2 = 0.9069 \quad \frac{G_1}{G_2} = \frac{G_1}{G_2} \cdot \frac{G_2}{G_1} = 0.6032 \xrightarrow{M_1} M_1 = 0.3093 \quad \frac{P_2}{P_1} = 0.936$$

$$\frac{P_2}{P_1} = 1.596 \quad \frac{P_2}{P_1} = 2.117 \quad \frac{A_1}{A_2} = 1.98$$

$$\frac{P_{01}}{P_0} = \frac{P_{01}}{A_1} \cdot \frac{A_1}{A_1^*} = \frac{A_1}{A_1^*} \cdot \frac{A_1}{A_1^*} = 0.8225 \rightarrow P_2 = \frac{P_2}{P_1} \cdot \frac{P_1}{P_1^*} \cdot \frac{P_{01}}{P_1} \cdot P_0 = 232.9 \text{ kPa}$$

Vari. Tot. + LS

$$P_0 = 100 \text{ kPa} \quad \text{Vergleichsraum}$$

$$P_{01} = 0.353 \rightarrow \frac{P_{01}}{P_{02}} = \frac{P_{01}}{P_{02}} = 1.177 \rightarrow P_2 = 250 \text{ kPa} \quad \frac{P_0}{P_{02}} = 0.4 \rightarrow M_0 = 1.22$$

$$\gamma = 4.14$$

$$\left[ \frac{G_1}{G_1^*} \cdot \frac{A_1}{A_1^*} = \frac{P_{01}}{P_{01}^*} \right]$$

$$P_0 = 100 \text{ kPa} \quad G_2/G_1 = 1.1$$

Reduktion der  $P_2$  der zu he. Prozessur zu  $t_1$

$$\frac{G_2}{G_1} = \frac{G_2}{G_1} \cdot \frac{G_1}{G_1^*} = 0.558 \rightarrow M_2 = 0.2806 \quad \frac{P_2}{P_1^*} = 2.162 \quad P_2 = 375.2 \text{ kPa} \rightarrow P_0 \text{ mehr strömung}$$

Prozessur zu  $P_2$

$$M_3 = 2.40 \xrightarrow{M_1} M_1 = 0.523 \rightarrow \frac{G_1}{G_1^*} = 0.851 \quad \frac{G_2}{G_1} = \frac{G_2}{G_1} \cdot \frac{G_1}{G_1^*} = 0.936 \xrightarrow{M_1} M_2 = 0.654$$

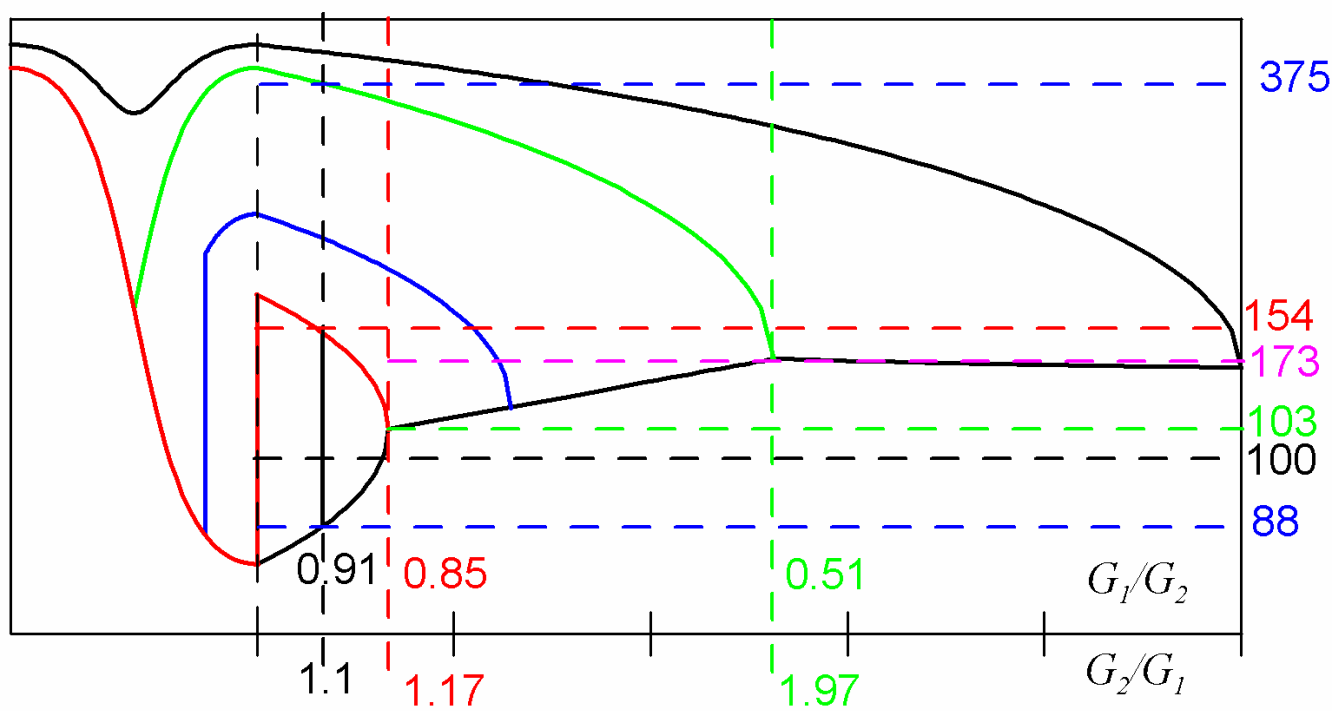
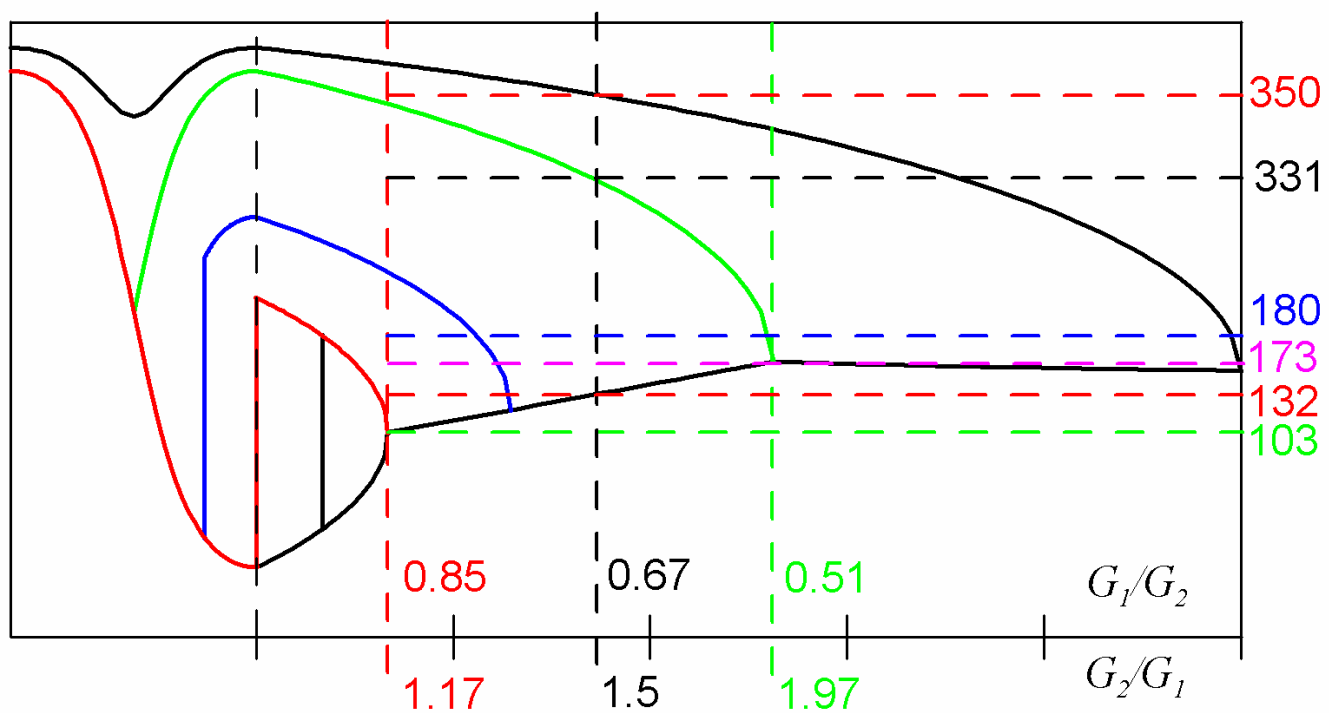
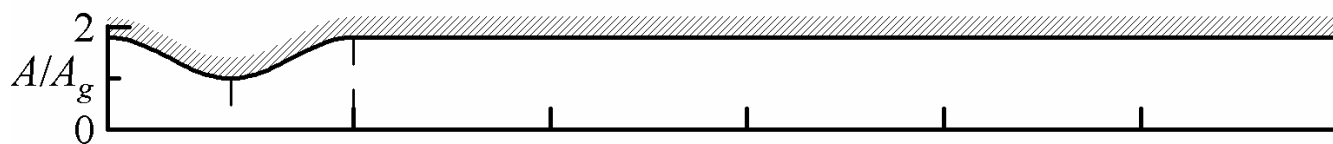
$$\frac{P_{01}}{P_0} = 0.5407 \quad \frac{P_2}{P_1^*} = 1.735 \quad \frac{P_2}{P_{01}^*} = 1.49$$

$$\frac{P_2}{P_{01}} = 0.830 \quad P_2 = \frac{P_2}{P_1^*} \cdot \frac{P_1^*}{P_1} \cdot \frac{P_{01}}{P_1} \cdot P_0 = 154.33 > P_0$$

Prozessur zu  $t_3$

$$\frac{G_2}{G_1} = \frac{G_2}{G_1} \cdot \frac{G_1}{G_1^*} = 0.9362 \rightarrow M_2 = 1.63 \quad \frac{P_2}{P_1^*} = 0.508 \quad P_2 = 52.5 \text{ kPa} < P_0 \rightarrow \text{only d'inter obscur}$$

$$\frac{P_0}{P_2} = 1.90 \xrightarrow{M_{2,3}} M_{2,3} = 1.33 \rightarrow M_{2,3} = 0.77 \quad E = 0.5 \quad \frac{M_{2,3}}{M_2} = 54.4\% \rightarrow$$



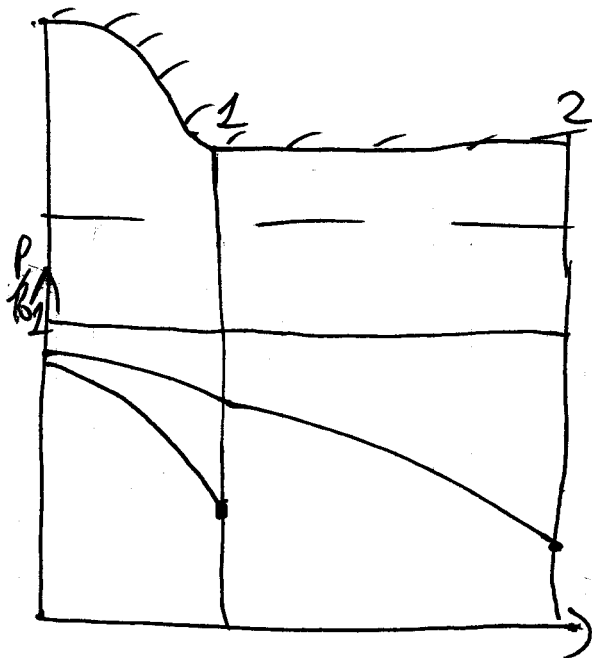
|          |           |                             |            |          |            |          |  |  |  |
|----------|-----------|-----------------------------|------------|----------|------------|----------|--|--|--|
| Dati     |           |                             |            |          |            |          |  |  |  |
| gamma    | 1.4       |                             |            |          | G2/G*      | 0.810866 |  |  |  |
| R        | 287       |                             | Condizioni | 1        | Condizioni | 2        |  |  |  |
| Po1      | 1.00E+06  | Pa                          | p/po       | 0.957453 | M          | 0.477471 |  |  |  |
| To1      | 500       | K                           | T/To       | 0.987654 | p/po       | 0.956393 |  |  |  |
| M1       | 0.25      |                             | p          | 9.57E+05 | T/To       | 0.845353 |  |  |  |
| G2/G1    | 1.6       | %                           | T          | 493.8272 |            |          |  |  |  |
|          |           |                             |            |          |            |          |  |  |  |
|          |           |                             | T/T*       | 1.185185 | T/T*       | 1.147671 |  |  |  |
|          |           |                             | p/p*       | 2.206897 | p/p*       | 1.819325 |  |  |  |
|          |           |                             | po/po*     | 1.217672 | po/po*     | 1.123439 |  |  |  |
|          |           |                             | G/G*       | 0.506791 |            |          |  |  |  |
|          |           |                             |            |          |            |          |  |  |  |
|          |           |                             |            |          | T2         | 478.1963 |  |  |  |
|          |           |                             |            |          | p2         | 7.89E+05 |  |  |  |
|          |           |                             |            |          | po2        | 9.23E+05 |  |  |  |
|          |           |                             |            |          |            |          |  |  |  |
| +++++    |           |                             |            |          |            |          |  |  |  |
| Dati     |           |                             |            |          |            |          |  |  |  |
| gamma    | 1.4       |                             |            |          |            |          |  |  |  |
| R        | 287       |                             |            |          | G2/G*      | 0.216185 |  |  |  |
| Po1      | 1.00E+06  | Pa                          | Condizioni | 1        | Condizioni | 2        |  |  |  |
| To1      | 500       | K                           | p/po       | 0.843019 | M          | 0.099955 |  |  |  |
| M1       | 0.5       |                             | T/To       | 0.952381 | p/po       | 0.998006 |  |  |  |
| G2/G1    | 0.26      | %                           | p          | 8.43E+05 | T/To       | 0.833887 |  |  |  |
|          |           |                             | T          | 476.1905 |            |          |  |  |  |
|          |           |                             |            |          |            |          |  |  |  |
|          |           |                             | T/T*       | 1.142857 | T/T*       | 1.197607 |  |  |  |
|          |           |                             | p/p*       | 1.777778 | p/p*       | 2.366893 |  |  |  |
|          |           |                             | po/po*     | 1.114053 | po/po*     | 1.259153 |  |  |  |
|          |           |                             | G/G*       | 0.831479 |            |          |  |  |  |
|          |           |                             |            |          |            |          |  |  |  |
|          |           |                             |            |          | T2         | 499.0029 |  |  |  |
|          |           |                             |            |          | p2         | 1.12E+06 |  |  |  |
|          |           |                             |            |          | po2        | 1.13E+06 |  |  |  |
|          |           |                             |            |          |            |          |  |  |  |
| Razzo    |           |                             |            |          |            |          |  |  |  |
| D        | 0.025     |                             |            |          |            |          |  |  |  |
| rpunto   | 0.025     |                             |            |          |            |          |  |  |  |
| rhop     | 2500      |                             |            |          |            |          |  |  |  |
| gamma    | 1.4       |                             |            |          |            |          |  |  |  |
| R        | 320       |                             |            |          |            |          |  |  |  |
| T        | 3000      |                             |            |          |            |          |  |  |  |
| L        | 0.3       |                             |            |          |            |          |  |  |  |
| Agola    | 0.0003    |                             |            |          |            |          |  |  |  |
|          |           |                             |            |          |            |          |  |  |  |
| psistar  | 0.8101852 |                             |            |          |            |          |  |  |  |
| port     | 1.4726216 |                             |            |          |            |          |  |  |  |
| Agrano   | 0.0004909 |                             |            |          |            |          |  |  |  |
| Ag/Agola | 1.6362462 |                             |            |          |            |          |  |  |  |
| Mgrano   | 0.3862991 |                             |            |          |            |          |  |  |  |
| T/To     | 1         | supponiamo che sia unitario |            |          |            |          |  |  |  |
| To       | 3000      |                             | e,f        |          |            |          |  |  |  |
| ao       | 1159.3101 |                             | G/G*       | 0.71045  |            |          |  |  |  |
| po       | 7024011.8 |                             | Ge         | 3000     |            |          |  |  |  |
| c,d      |           |                             | G*         | 4222.675 |            |          |  |  |  |
| po/po*   | 1.1624713 |                             | pe/poe     | 0.90219  |            |          |  |  |  |
| M        | 0         |                             | pe         | 6336991  |            |          |  |  |  |
| po/po*   | 1.2678763 |                             | deltap     | -1323910 |            |          |  |  |  |
| Poin     | 7660901.8 |                             |            |          |            |          |  |  |  |
| rho      | 7.980106  |                             |            |          |            |          |  |  |  |

|                                             |           |          |          |          |           |          |          |             |          |
|---------------------------------------------|-----------|----------|----------|----------|-----------|----------|----------|-------------|----------|
|                                             |           |          |          |          |           |          |          |             |          |
|                                             |           |          |          |          |           |          |          |             |          |
| Ugello convergente condotto adduzione massa |           |          |          |          |           |          |          |             |          |
| Dati                                        |           |          |          |          |           |          |          |             |          |
| gamma                                       | 1.4       |          |          |          |           |          |          |             |          |
| R                                           | 287       |          |          |          |           |          |          |             |          |
| Po1                                         | 125 kPa   |          |          |          |           |          |          |             |          |
| To1                                         | 350 K     |          |          |          |           |          |          |             |          |
| pa                                          | 100 kPa   |          |          |          |           |          |          |             |          |
| G2/G1                                       | 1.6 %     |          |          |          |           |          |          |             |          |
|                                             |           |          |          |          |           |          |          |             |          |
| M2                                          | G/G*      | p/p*     | G1/G*    | M1       | p/po      | p/p*     | p2       | Err         | M2       |
| 1                                           | 1         | 1        | 0.625    | 0.323759 | 0.9299583 | 2.092875 | 55.54312 | -0.44456879 | 0.8      |
| 0.8                                         | 0.9818086 | 1.265823 | 0.61363  | 0.316125 | 0.9330797 | 2.105431 | 70.12303 | -0.2987697  | 0.390162 |
| 0.390162                                    | 0.7152794 | 1.978374 | 0.44705  | 0.216418 | 0.9678936 | 2.252313 | 106.2716 | 0.06271628  | 0.461268 |
| 0.461268                                    | 0.7950417 | 1.849177 | 0.496901 | 0.2443   | 0.9593201 | 2.21493  | 100.1133 | 0.00113345  | 0.462576 |
| 0.462576                                    | 0.7963512 | 1.846768 | 0.49772  | 0.24477  | 0.9591678 | 2.214273 | 99.99673 | -3.2739E-05 | 0.46254  |
| 0.46254                                     | 0.7963145 | 1.846836 | 0.497697 | 0.244757 | 0.9591721 | 2.214292 | 100      | 1.2529E-08  | 0.46254  |
| 0.46254                                     | 0.7963146 | 1.846836 | 0.497697 | 0.244757 | 0.9591721 | 2.214292 | 100      | 1.3799E-13  | 0.46254  |
| 0.46254                                     | 0.7963146 | 1.846836 | 0.497697 | 0.244757 | 0.9591721 | 2.214292 | 100      | -4.2633E-16 | 0.46254  |

|                                   |            |          |          |                              |           |          |          |                 |          |     |    |
|-----------------------------------|------------|----------|----------|------------------------------|-----------|----------|----------|-----------------|----------|-----|----|
| Ugello convergente-divergente     |            |          |          |                              |           |          |          |                 |          |     |    |
| Dati                              |            |          |          |                              |           |          |          |                 |          |     |    |
| gamma                             | 1.4        |          |          |                              |           |          |          |                 |          |     |    |
| R                                 | 287        |          |          |                              |           |          |          |                 |          |     |    |
| Po1                               | 400        |          |          |                              |           |          |          |                 |          |     |    |
| To1                               | 350        |          |          |                              |           |          |          |                 |          |     |    |
|                                   |            | kPa      |          |                              |           |          |          |                 |          |     |    |
| A/A*                              | 2.4        |          |          |                              |           |          |          |                 |          |     |    |
| Sup                               |            | Sub      |          |                              |           |          |          |                 |          |     |    |
| M                                 | 2.3985993  | M        | 0.250305 |                              |           |          |          |                 |          |     |    |
| G/G*                              | 0.85112819 | G/G*     | 0.507317 |                              |           |          |          |                 |          |     |    |
| p/po                              | 0.06854912 | p/po     | 0.957352 |                              |           |          |          |                 |          |     |    |
| p/p*                              | 0.26505893 | p/p*     | 2.206463 |                              |           |          |          |                 |          |     |    |
| p*/po                             | 0.2586184  | p*/po    | 0.433885 |                              |           |          |          |                 |          |     |    |
| p*                                | 103.44736  | p*       | 173.5541 |                              |           |          |          |                 |          |     |    |
|                                   |            |          |          |                              |           |          |          |                 |          |     |    |
| Dati                              |            |          |          |                              |           |          |          |                 |          |     |    |
| pa                                | 350        | kPa      |          |                              |           |          |          |                 |          |     |    |
| G2/G1                             | 1.5        | G1/G2    | 0.666667 |                              |           |          |          |                 |          |     |    |
| Supponedo di passare per r1 si ha |            |          |          |                              |           |          | 1.217561 | 1.23459588      |          |     |    |
| G2/G*                             | M2         | p/p*     | p2       |                              |           |          | 1.013991 |                 |          |     |    |
| 0.7609757                         | 0.42900946 | 1.908293 | 331.192  | minore pa moto non strozzato |           |          |          |                 |          |     |    |
| M2                                | G/G*       | p/p*     | G1/G*    | M1                           | p/po      | p/p*     | p2       | Err             | M2       |     |    |
| 0.4290095                         | 0.76097566 | 1.908293 | 0.507317 | 0.250305                     | 0.9573519 | 2.206463 | 331.192  | -0.05373712     | 0.2      |     |    |
| 0.2                               | 0.41659779 | 2.272727 | 0.277732 | 0.129527                     | 0.988344  | 2.344922 | 383.1661 | 0.0947602       | 0.346137 |     |    |
| 0.3461372                         | 0.6571529  | 2.05526  | 0.438102 | 0.211549                     | 0.9692935 | 2.258495 | 352.8279 | 0.00807967      | 0.359759 |     |    |
| 0.3597589                         | 0.67586389 | 2.031837 | 0.450576 | 0.218347                     | 0.9673308 | 2.249833 | 349.4407 | -0.00159788     | 0.35751  |     |    |
| 0.3575098                         | 0.67281941 | 2.035729 | 0.448546 | 0.217236                     | 0.9676555 | 2.251263 | 350.0052 | 1.4914E-05      | 0.357531 |     |    |
| 0.3575306                         | 0.67284765 | 2.035694 | 0.448565 | 0.217246                     | 0.9676525 | 2.25125  | 350      | 2.65E-08        | 0.357531 |     |    |
| 0.3575307                         | 0.6728477  | 2.035693 | 0.448565 | 0.217246                     | 0.9676525 | 2.25125  | 350      | -4.4289E-13     | 0.357531 |     |    |
| 0.3575307                         | 0.6728477  | 2.035693 | 0.448565 | 0.217246                     | 0.9676525 | 2.25125  | 350      | -1.6241E-16     | 0.357531 |     |    |
|                                   |            |          |          |                              |           |          |          |                 |          |     |    |
| Dati                              |            |          |          |                              |           |          |          |                 |          |     |    |
| pa                                | 180        | kPa      |          |                              |           |          |          |                 |          |     |    |
| G2/G1                             | 1.5        | G1/G2    | 0.666667 |                              |           |          |          |                 |          |     |    |
| Supponedo di passare per r1 si ha |            |          |          |                              |           |          |          |                 |          |     |    |
| G2/G*                             | M2         | p/p*     | p2       |                              |           |          |          |                 |          |     |    |
| 0.7609757                         | 0.42900946 | 1.908293 | 331.192  | maggiore pa moto strozzato   |           |          |          |                 |          |     |    |
| Supponendo M2 =1 ond d'urto       |            |          |          |                              |           |          |          |                 |          |     |    |
| M2                                | G1/G*      | M1       | p/po     | A/A*                         | po1/po    | p/p*     | p2       |                 |          |     |    |
| 1                                 | 0.66666667 | 0.353004 | 0.917448 | 1.76502                      | 0.7354249 | 2.043498 | 132.0704 | < pa ond d'urto |          |     |    |
| M2                                | G/G*       | p/p*     | G1/G*    | M1                           | p/po      | A/A*     | po1/po   | p/p*            | p2       | Err | M2 |

|                                   |            |          |          |                               |           |          |          |               |                 |              |          |
|-----------------------------------|------------|----------|----------|-------------------------------|-----------|----------|----------|---------------|-----------------|--------------|----------|
| 1                                 | 1          | 1        | 0.666667 | 0.353004                      | 0.9174483 | 1.76502  | 0.735425 | 2.04349839    | 132.0704        | -0.266275295 | 0.429009 |
| 0.4290095                         | 0.76097566 | 1.908293 | 0.507317 | 0.250305                      | 0.9573519 | 2.4      | 1        | 2.20646323    | 331.192         | 0.8399556    | 0.86256  |
| 0.8625597                         | 0.99210797 | 1.175541 | 0.661405 | 0.349192                      | 0.9191277 | 1.781494 | 0.742289 | 2.05004014    | 156.4893        | -0.13061524  | 0.804214 |
| 0.8042144                         | 0.98266651 | 1.259535 | 0.655111 | 0.344679                      | 0.9210971 | 1.801511 | 0.75063  | 2.0577457     | 169.2816        | -0.059546721 | 0.755328 |
| 0.7553282                         | 0.97107658 | 1.334276 | 0.647384 | 0.339208                      | 0.9234574 | 1.826557 | 0.761065 | 2.06702914    | 181.467         | 0.0081501    | 0.761214 |
| 0.7612136                         | 0.97266972 | 1.32507  | 0.648446 | 0.339955                      | 0.9231367 | 1.823082 | 0.759618 | 2.06576435    | 179.9199        | -0.000445076 | 0.760909 |
| 0.7609089                         | 0.97258861 | 1.325546 | 0.648392 | 0.339917                      | 0.923153  | 1.823259 | 0.759691 | 2.06582882    | 179.9994        | -3.15906E-06 | 0.760907 |
| 0.7609067                         | 0.97258803 | 1.325549 | 0.648392 | 0.339917                      | 0.9231531 | 1.82326  | 0.759692 | 2.06582928    | 180             | 1.23306E-09  | 0.760907 |
|                                   |            |          |          |                               |           |          |          |               |                 |              |          |
| Dati                              |            |          |          |                               |           |          |          |               |                 |              |          |
| pa                                | 100        | kPa      |          |                               |           |          |          |               |                 |              |          |
| G2/G1                             | 1.5        | G1/G2    | 0.666667 |                               |           |          |          |               |                 |              |          |
| Supponedo di passare per r1 si ha |            |          |          |                               |           |          |          |               |                 |              |          |
| G2/G*                             | M2         | p/p*     | p2       |                               |           |          |          |               |                 |              |          |
| 0.7609757                         | 0.42900946 | 1.908293 | 331.192  | maggiore pa moto strozzato    |           |          |          |               |                 |              |          |
| Supponendo M2 =1                  |            |          |          |                               |           |          |          |               |                 |              |          |
| M2                                | G1/G*      | M1       | p/po     | A/A*                          | po1/po    | p/p*     | p2       |               | po1/po2=po1/po* |              |          |
| 1                                 | 0.66666667 | 0.353004 | 0.917448 | 1.76502                       | 0.7354249 | 2.043498 | 132.0704 | >pa ventaglio | 1.17668         |              |          |
|                                   |            |          |          |                               |           |          |          |               |                 |              |          |
| po2                               | pa/po2     | Ma       | ni       |                               |           |          |          |               |                 |              |          |
| 250                               | 0.4        | 1.22324  | 4.139316 |                               | 1.1766799 |          |          |               |                 |              |          |
|                                   |            |          |          |                               |           |          |          |               |                 |              |          |
|                                   |            |          |          |                               |           |          |          |               |                 |              |          |
| Dati                              |            |          |          |                               |           |          |          |               |                 |              |          |
| pa                                | 100        | kPa      |          |                               |           |          |          |               |                 |              |          |
| G2/G1                             | 1.1        | G1/G2    | 0.909091 |                               |           |          |          |               |                 |              |          |
| Supponedo di passare per r1 si ha |            |          |          |                               |           |          |          |               |                 |              |          |
| G2/G*                             | M2         | p/p*     | p2       |                               |           |          |          |               |                 |              |          |
| 0.5580488                         | 0.28058765 | 2.161731 | 375.1773 | maggiore pa moto strozzato    |           |          |          |               |                 |              |          |
| Supponedo di passare per r2 si ha |            |          |          |                               |           |          |          |               |                 |              |          |
| M1                                | po1/po     | G/G*     | p/po1    | p/p*                          | G2/G*     | M2       | p/p*     | p2            |                 |              |          |
| 0.5232674                         | 0.54073497 | 0.851128 | 0.829774 | 1.734941                      | 0.936241  | 0.659375 | 1.491902 | 154.333308    |                 |              |          |
| Supponedo di passare per r3 si ha |            |          |          |                               |           |          |          |               |                 |              |          |
| G2/G*                             | M2         | p/p*     | p2       |                               |           |          |          |               |                 |              |          |
| 0.936241                          | 1.63084045 | 0.508098 | 52.56141 | minore pa onda d'urto obliqua |           |          |          |               |                 |              |          |
| pa/p2                             | Mn2        | Mnv      | eps      |                               |           |          |          |               |                 |              |          |
| 1.9025364                         | 1.33176673 | 0.770314 | 54.74724 |                               |           |          |          |               |                 |              |          |

Moto con riduzione di Massa



$$\gamma = 1.4 \quad R = 287 \frac{\text{J}}{\text{kg} \cdot \text{K}} \quad P_2 = 70 \times P_0$$

$$D_1 = D_2 = 0.05 \text{ m} \quad P_0 = 100 \times P_2$$

$$T_0 = 350 \text{ K}$$

Considerando solo l'ugello  
Per moto stazionario v. ho:

$$\dot{m} = \frac{P_0 A_1 \Psi^+}{Q_0} \Rightarrow G_u^* = \frac{\dot{m}}{A_1} = \frac{P_0 \Psi^+}{Q_0} =$$

$$G_u^* = \frac{100 \cdot 0.81 \cdot 10^3}{\sqrt{1.4 \cdot 287 \cdot 350}} = 0.216 \frac{\text{kg}}{\text{m}^2 \cdot \text{s}}$$

Supponiamo che la massa aggiunta  
sia il 20% di  $G_u^*$

$$\Delta G = G_u^* \cdot 0.2 = 0.0432 \frac{\text{kg}}{\text{m}^2 \cdot \text{s}}$$

Si procede per tentativi. Supponiamo  $M_1 = 0.2$

$$M_1 = 0.2 \xrightarrow{M_1} P_1/P_0 = 2.27$$

$$\downarrow 150 \quad G_1 = 0.417$$

$$\frac{P_1}{P_0} = 0.973$$

$$\frac{A_1}{A^*} = 2.96 \rightarrow G_1 = G_u^* \frac{A_1^*}{A_1} = \frac{0.216}{2.96} = 0.0729 \frac{\text{kg}}{\text{m}^2 \cdot \text{s}} \quad \Delta G = 0.593$$

$$\frac{G_2}{G_1} = \frac{\Delta G + G_1}{G_1} = 1 + \frac{\Delta G}{G_1} = 1.593 \rightarrow \frac{G_2}{G_1^*} = \frac{G_2}{G_1} \frac{G_1}{G_1^*} = 1.59 \cdot 0.417 = 0.664$$

$$\frac{G_2}{G_1^*} = 0.664 \xrightarrow{M_2} M_2 = 0.351$$

$$\frac{P_2}{P_1} = 2.05$$

$$P_2 = \frac{P_2}{P_1} \frac{P_1}{P_0} = \frac{2.05}{2.27} \cdot 100 = 87.6$$

$$M_1 = 0.25 \xrightarrow{M_1} P_1/P_0 = 2.21 \quad G_1/G_1^* = 0.507$$

$$\downarrow 150$$

$$\frac{P_1}{P_0} = 0.973 \quad \frac{A_1}{A^*} = 2.40 \quad G_1 = 0.0899 \quad \frac{\Delta G}{G_1} = 0.481$$

$$\frac{G_2}{G_1} = 1.48 \quad \frac{G_2}{G_1^*} = 0.750 \xrightarrow{M_2} M_2 = 0.420 \quad P_2 = 83.56$$

$$\frac{P_2}{P_1} = 1.43$$

Verif. Tab.



S<sub>2</sub> e Suppore  $M_2 = 0.4 \rightarrow \frac{P_2}{P_1} = 1.96$

$$\frac{G_2}{G^*} = 0.727$$

S<sub>1</sub> Suppore  $G_1 = Q \cdot G_2^*$  con  $Q = 0.3$   $\frac{G_2}{G_1} = \frac{0.432}{0.3 \cdot 0.28} = 0.667$

$\frac{G_2}{G_1} = 1.67$   $\frac{G_1}{G_2} = \frac{G_1}{G_2} \cdot \frac{G_2}{G_1} = \frac{0.727}{1.67} = 0.436 \xrightarrow{M_2} M_1 = 0.21 \rightarrow \frac{P_1}{P_2} = 0.970$   
 $\frac{P_1}{P_2} = 2.26$   $\frac{A_2}{A_1} = 2.82$

$G_1 = G_2^* \frac{A_1}{A_2} = \frac{0.216}{2.82} = 0.0766 \frac{kg}{m^2 s}$   $Q = \frac{G_1}{G_2^*} = \frac{A_1}{A_2} = \frac{1}{2.82} = 0.354$

S<sub>1</sub> itera con  $Q = 0.4$  (Verli Tab)

Dopo 3 iterazioni si trova  $Q = 0.395$  e  $M_1 = 0.236$   $\frac{P_1}{P_2} = 0.982$   
 $\frac{P_1}{P_2} = 2.13$

Altro iterazione con  $M_2 = 0.3$

$P_0 = 99.7$   $P_2 = 84.7$

Verli Tab

|                |         |         |         |           |         |         |                |         |                |         |         |                |                |         |         |                |           |
|----------------|---------|---------|---------|-----------|---------|---------|----------------|---------|----------------|---------|---------|----------------|----------------|---------|---------|----------------|-----------|
| gamma          | 1.4     |         |         | pa        | 70      | kPa     |                |         |                |         |         |                |                |         |         |                |           |
| R              | 287     |         |         | G* ugello | 0.216   |         |                |         |                |         |         |                |                |         |         |                |           |
| Po1            | 100     | kPa     |         | perc DG   | 20%     |         |                |         |                |         |         |                |                |         |         |                |           |
| To1            | 350     | K       |         | DeltaG    | 0.0432  |         |                |         |                |         |         |                |                |         |         |                |           |
| D              | 0.05    | m       |         | A1        | 0.00196 |         |                |         |                |         |         |                |                |         |         |                |           |
| <b>M1</b>      | p1/p*   | G1/G*   | p1/p01  | Au/A*     | G1      | DG/G1   | G2/G1          | G2/G*   | <b>M2</b>      | p2/p*   | p2      | <b>Err</b>     |                |         |         |                |           |
| <b>0.2</b>     | 2.27273 | 0.4166  | 0.9725  | 2.96352   | 0.07289 | 0.5927  | 1.5927         | 0.66352 | <b>0.35072</b> | 2.04743 | 87.609  | <b>17.609</b>  | 0.25           |         |         |                |           |
| <b>0.25</b>    | 2.2069  | 0.50679 | 0.95745 | 2.40271   | 0.0899  | 0.48054 | 1.48054        | 0.75033 | <b>0.41955</b> | 1.9255  | 83.5368 | <b>13.5368</b> | 0.41621        |         |         |                |           |
| <b>0.41621</b> | 1.93155 | 0.74649 | 0.88762 | 1.53999   | 0.14026 | 0.308   | 1.308          | 0.97641 | <b>0.77593</b> | 1.30229 | 59.8454 | <b>-10.155</b> | 0.34497        |         |         |                |           |
| <b>0.34497</b> | 2.05725 | 0.65552 | 0.92097 | 1.8002    | 0.11998 | 0.36004 | 1.36004        | 0.89153 | <b>0.57858</b> | 1.63414 | 73.1557 | <b>3.15565</b> | 0.36186        |         |         |                |           |
| <b>0.36186</b> | 2.02819 | 0.67869 | 0.91349 | 1.72821   | 0.12498 | 0.34564 | 1.34564        | 0.91328 | <b>0.61435</b> | 1.57028 | 70.7248 | <b>0.72483</b> | 0.3669         |         |         |                |           |
| <b>0.3669</b>  | 2.01942 | 0.68541 | 0.91121 | 1.70815   | 0.12645 | 0.34163 | 1.34163        | 0.91956 | <b>0.6258</b>  | 1.55012 | 69.9448 | <b>-0.0552</b> | 0.36654        |         |         |                |           |
| <b>0.36654</b> | 2.02005 | 0.68494 | 0.91137 | 1.70955   | 0.12635 | 0.34191 | 1.34191        | 0.91912 | <b>0.62497</b> | 1.55156 | 70.0009 | <b>0.00095</b> | 0.36655        |         |         |                |           |
| <b>0.36655</b> | 2.02003 | 0.68494 | 0.91137 | 1.70953   | 0.12635 | 0.34191 | 1.34191        | 0.91913 | <b>0.62499</b> | 1.55154 | 70      | <b>1.2E-06</b> | 0.36655        |         |         |                |           |
| <b>0.36655</b> | 2.02003 | 0.68494 | 0.91137 | 1.70953   | 0.12635 | 0.34191 | 1.34191        | 0.91913 | <b>0.62499</b> | 1.55154 | 70      | <b>-3E-11</b>  | 0.36655        |         |         |                |           |
| <b>0.36655</b> | 2.02003 | 0.68494 | 0.91137 | 1.70953   | 0.12635 | 0.34191 | 1.34191        | 0.91913 | <b>0.62499</b> | 1.55154 | 70      | <b>0</b>       | 0.36655        |         |         |                |           |
|                |         |         |         |           |         |         |                |         |                |         |         |                |                |         |         |                |           |
| <b>M2</b>      | p2/p*   | G2/G*   | %G1     | DG/G1     | G2/G1   | G1/G*   | <b>M1</b>      | p1/p*   | p1/p01         | Au/A*   | G1      | %G1            | <b>Err</b>     | %G1     | p2      | <b>Err</b>     | <b>M1</b> |
| 0.4            | 1.96078 | 0.72734 | 0.3     | 0.66667   | 1.66667 | 0.43641 | <b>0.21063</b> | 2.25965 | 0.96955        | 2.82127 | 0.07656 | 0.35445        | <b>0.05445</b> | 0.35    |         |                |           |
| 0.4            | 1.96078 | 0.72734 | 0.35    | 0.57143   | 1.57143 | 0.46285 | <b>0.22511</b> | 2.24101 | 0.96532        | 2.64968 | 0.08152 | 0.3774         | <b>0.0274</b>  | 0.40066 |         |                |           |
| 0.4            | 1.96078 | 0.72734 | 0.40066 | 0.49917   | 1.49917 | 0.48516 | <b>0.23761</b> | 2.22419 | 0.96146        | 2.51895 | 0.08575 | 0.39699        | <b>-0.0037</b> | 0.39468 |         |                |           |
| 0.4            | 1.96078 | 0.72734 | 0.39468 | 0.50674   | 1.50674 | 0.48273 | <b>0.23623</b> | 2.22608 | 0.9619         | 2.53267 | 0.08528 | 0.39484        | <b>0.00016</b> | 0.39493 | 84.7262 | <b>14.7262</b> | 0.3       |
| 0.3            | 2.13144 | 0.58895 | 0.39493 | 0.50642   | 1.50642 | 0.39096 | <b>0.18649</b> | 2.28857 | 0.97603        | 3.16835 | 0.06817 | 0.31562        | <b>-0.0793</b> | 0.39468 |         |                |           |
| 0.3            | 2.13144 | 0.58895 | 0.39468 | 0.50674   | 1.50674 | 0.39088 | <b>0.18645</b> | 2.28862 | 0.97604        | 3.16907 | 0.06816 | 0.31555        | <b>-0.0791</b> | 0.28449 |         |                |           |
| 0.3            | 2.13144 | 0.58895 | 0.28449 | 0.703     | 1.703   | 0.34583 | <b>0.16331</b> | 2.31362 | 0.98155        | 3.60066 | 0.05999 | 0.27773        | <b>-0.0068</b> | 0.27419 |         |                |           |
| 0.3            | 2.13144 | 0.58895 | 0.27419 | 0.72942   | 1.72942 | 0.34055 | <b>0.16064</b> | 2.31632 | 0.98214        | 3.65857 | 0.05904 | 0.27333        | <b>-0.0009</b> | 0.27269 | 90.3753 | <b>20.3753</b> | 0.66068   |
| 0.66068        | 1.48967 | 0.93684 | 0.27269 | 0.73343   | 1.73343 | 0.54045 | <b>0.26988</b> | 2.17792 | 0.95064        | 2.23941 | 0.09645 | 0.44655        | <b>0.17386</b> | 0.27418 |         |                |           |
| 0.66068        | 1.48967 | 0.93684 | 0.27418 | 0.72944   | 1.72944 | 0.5417  | <b>0.27063</b> | 2.1768  | 0.95038        | 2.23372 | 0.0967  | 0.44768        | <b>0.1735</b>  | 1.00134 |         |                |           |
| 0.66068        | 1.48967 | 0.93684 | 1.00134 | 0.19973   | 1.19973 | 0.78087 | <b>0.44745</b> | 1.87457 | 0.87161        | 1.45501 | 0.14845 | 0.68728        | <b>-0.3141</b> | 0.53295 |         |                |           |
| 0.66068        | 1.48967 | 0.93684 | 0.53295 | 0.37527   | 1.37527 | 0.6812  | <b>0.36373</b> | 2.02493 | 0.91265        | 1.72067 | 0.12553 | 0.58117        | <b>0.04822</b> | 0.59529 | 67.1399 | <b>-2.8601</b> | 0.61628   |
| 0.61628        | 1.56686 | 0.91436 | 0.59529 | 0.33597   | 1.33597 | 0.68442 | <b>0.36615</b> | 2.02073 | 0.91155        | 1.71109 | 0.12623 | 0.58442        | <b>-0.0109</b> | 0.58383 |         |                |           |
| 0.61628        | 1.56686 | 0.91436 | 0.58383 | 0.34257   | 1.34257 | 0.68105 | <b>0.36362</b> | 2.02513 | 0.9127         | 1.72112 | 0.1255  | 0.58102        | <b>-0.0028</b> | 0.57983 |         |                |           |
| 0.61628        | 1.56686 | 0.91436 | 0.57983 | 0.34493   | 1.34493 | 0.67986 | <b>0.36273</b> | 2.02668 | 0.9131         | 1.7247  | 0.12524 | 0.57981        | <b>-2E-05</b>  | 0.5798  |         |                |           |
| 0.61628        | 1.56686 | 0.91436 | 0.5798  | 0.34495   | 1.34495 | 0.67985 | <b>0.36272</b> | 2.02669 | 0.9131         | 1.72473 | 0.12523 | 0.5798         | <b>-4E-08</b>  | 0.5798  | 70.593  | <b>0.59302</b> | 0.62391   |
| 0.62391        | 1.55343 | 0.91855 | 0.5798  | 0.34495   | 1.34495 | 0.68296 | <b>0.36506</b> | 2.02263 | 0.91205        | 1.71541 | 0.12591 | 0.58295        | <b>0.00315</b> | 0.5798  |         |                |           |
| 0.62391        | 1.55343 | 0.91855 | 0.5798  | 0.34495   | 1.34495 | 0.68296 | <b>0.36506</b> | 2.02263 | 0.91205        | 1.71541 | 0.12591 | 0.58295        | <b>0.00315</b> | 0.58434 |         |                |           |
| 0.62391        | 1.55343 | 0.91855 | 0.58434 | 0.34227   | 1.34227 | 0.68433 | <b>0.36608</b> | 2.02085 | 0.91158        | 1.71136 | 0.12621 | 0.58433        | <b>-7E-06</b>  | 0.58433 |         |                |           |
| 0.62391        | 1.55343 | 0.91855 | 0.58433 | 0.34227   | 1.34227 | 0.68432 | <b>0.36608</b> | 2.02085 | 0.91158        | 1.71137 | 0.12621 | 0.58433        | <b>1.6E-08</b> | 0.58433 | 70.0735 | <b>0.0735</b>  | 0.62499   |
| 0.62499        | 1.55154 | 0.91913 | 0.58433 | 0.34227   | 1.34227 | 0.68476 | <b>0.3664</b>  | 2.02028 | 0.91143        | 1.71008 | 0.12631 | 0.58477        | <b>0.00044</b> | 0.58433 |         |                |           |
| 0.62499        | 1.55154 | 0.91913 | 0.58433 | 0.34227   | 1.34227 | 0.68476 | <b>0.3664</b>  | 2.02028 | 0.91143        | 1.71008 | 0.12631 | 0.58477        | <b>0.00044</b> | 0.58496 |         |                |           |
| 0.62499        | 1.55154 | 0.91913 | 0.58496 | 0.34191   | 1.34191 | 0.68494 | <b>0.36655</b> | 2.02003 | 0.91137        | 1.70953 | 0.12635 | 0.58496        | <b>-1E-07</b>  | 0.58496 |         |                |           |
| 0.62499        | 1.55154 | 0.91913 | 0.58496 | 0.34191   | 1.34191 | 0.68494 | <b>0.36655</b> | 2.02003 | 0.91137        | 1.70953 | 0.12635 | 0.58496        | <b>4.3E-11</b> | 0.58496 | 70      | <b>-1E-05</b>  | 0.62499   |