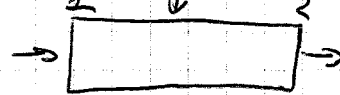


M₁₀ con addezione di NO₂

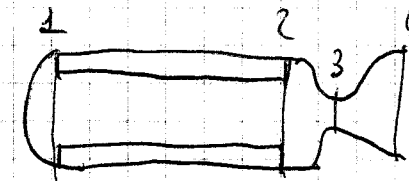


$\delta = 1.4, R = 287, P_0 = 1000 \text{ kPa}, T_0 = 500 \text{ K}, M_1 = 0.15, G_2/G_1 = 1.6$

$M_1 = 0.15 \xrightarrow{ISO} P_1/P_0 = 0.957, T_1/T_0 = 0.988 \rightarrow P_1 = 9.57 \cdot 10^5 \text{ Pa}, T_1 = 493.8 \text{ K}$
 $\xrightarrow{M_1} \frac{P_1}{P^*} = 1.185, \frac{P_1}{P^*} = 2.207, \frac{P_1}{P^*} = 1.218, \frac{G_1}{G^*} = 0.8668$

$\frac{G_2}{G^*} = \frac{G_2}{G_1} \frac{G_1}{G^*} = 0.8108 \xrightarrow{M_2} M_2 = 0.647, \frac{T_2}{T^*} = \frac{P_2/P^*}{P_1/P^*} = \frac{P_2/P_1}{P_1/P^*}$
 $\left. \begin{matrix} T_2 = 478 \\ P_2 = ? \end{matrix} \right\}$

$M_1 = 0.5, G_2/G_1 = 0.86$ come sopra

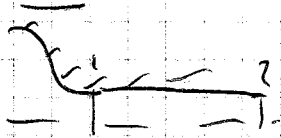


$D_1 = 0.075 \text{ m}, L_{12} = 0.30 \text{ m}, T_{\text{Fanno}} = 3000 \text{ K}, \dot{m} = ? (P_2 - P_1)$
 $\dot{V} = 0.025 \text{ m/s}, R = 320 \text{ J/kgK}, A_3 = 3.00 \cdot 10^{-4} \text{ m}^2, R_2 = ?, P_1 = ?, G^*$
 $\rho = 2500 \text{ kg/m}^3, \delta = 1.4$

$\dot{m} = \dot{V} \rho = \pi D \cdot L = 1.473 \text{ kg/s}$
 $A_1 = \pi D^2/4 = 4.909 \cdot 10^{-4} \text{ m}^2 \rightarrow \frac{A_1}{A_3} = 1.636 \xrightarrow{ISO} M_2 = 0.386$
 $\frac{P_2}{P^*} = 1.16, \frac{G_2}{G^*} = 0.7105$
 $Q_0 = \sqrt{\delta R T_0} = 1159 \text{ m/s}$
 $\boxed{P_0 = \frac{\dot{m} Q_0}{A_3 \gamma^*} = 7024 \text{ kPa}}$
 $S_{\text{supra}} \text{ de } T_{\text{Fanno}} = T_0 \text{ sensore}$

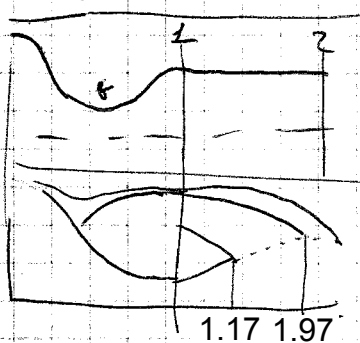
$M_1 = 0 \rightarrow \frac{P_0}{P^*} = 1.268, \boxed{P_0 = \frac{P_0}{P^*} \frac{P^*}{P_2} P_2 = 7661 \text{ kPa}}, G_2 = \frac{\dot{m}}{A_2} = 3000 \frac{\text{kg}}{\text{s}} \frac{1}{\pi \cdot 22} \Rightarrow G^* = 6223 \frac{\text{kg}}{\text{s} \cdot \text{m}^2}$

$P_2 = \frac{P_0}{P^*} P^* P_2 = 6337 \text{ kPa}, \Delta P = P_2 - P_1 = P_2 - P_1 = 1326 \text{ kPa}$



$\delta = 1.4, R = 287, P_0 = 125 \text{ kPa}, T_0 = 350 \text{ K}, P_a = 100 \text{ kPa}, G_2/G_1 = 1.6$
 $M_2 = 1 \rightarrow \frac{G_2}{G^*} = 1, \frac{P_2}{P^*} = 1$
 $\frac{G_2}{G^*} = \frac{G_1}{G^*} \frac{G_2}{G_1} = 0.625$
 $M_1 = 0.324 \xrightarrow{ISO} \frac{P_1}{P^*} = 0.9300, \frac{P_1}{P^*} = 2.093$
 $P_2 = \frac{P_0}{P^*} \frac{P^*}{P_1} P_1 = 55.54 \text{ kPa}$

Vedi Tabella E10.2



$\delta = 1.4, R = 287, P_0 = 600 \text{ kPa}, T_0 = 350 \text{ K}, A_1/A_0 = 2.4$

$\frac{A_1}{A_0} \xrightarrow{M_1} M_1 = 2.60 \xrightarrow{M^*} \frac{G_1}{G^*} = 0.851 = 1/1.17, M_1 = 0.250, \frac{G_1}{G^*} = 0.507$
 $\frac{P_1}{P^*} = 0.0685, \frac{P_1}{P^*} = 0.265, \frac{P_1}{P^*} = 0.457, \frac{P_1}{P^*} = 2.206$
 $P^* = 103.65, \frac{P^*}{P_0} = 0.1759, P^* = 173.35, \frac{P^*}{P_0} = 0.4339$

$P_0 = 350, G_2/G_1 = 1.5$ Velocità de P_2 de n'he pannello per t_1

$\frac{G_2}{G^*} = \frac{G_2}{G_1} \frac{G_1}{G^*} = 0.761 \xrightarrow{M_2} M_2 = 0.624 \rightarrow P_2 = 331.142 < P_0$ Tant'è che come sopra
 $\frac{P_2}{P^*} = 1.408$

$P_0 = 180 \text{ kPa}$ Velocità P_2 ~~supra~~ $M_2 = 1, \frac{G_1}{G^*} = \frac{1}{1.5} = 0.666 \rightarrow M_1 = 0.333 \xrightarrow{ISO} \frac{P_1}{P^*} = 0.4174, \frac{P_1}{P^*} = 2.044, \frac{A_1}{A^*} = 1.765$

$\frac{P_0}{P^*} = \frac{A^*}{A^*} = \frac{A}{A^*} \frac{A^*}{A_1} = 0.7334, P_2 = \frac{P_0}{P^*} \frac{P^*}{P_1} P_1 = 132.1 < P_0 \rightarrow \text{ONDA D'URTO}$

$$M_2 = 0.6 \xrightarrow{M_1} G_2 = 0.9069 \quad \frac{G_1}{G_2} = \frac{G_1}{G_2} \cdot \frac{G_2}{G_1} = 0.6032 \xrightarrow{M_1} M_1 = 0.3093 \quad \frac{P_2}{P_1} = 0.936$$

$$\frac{P_2}{P_1} = 1.596 \quad \frac{P_2}{P_1} = 2.117 \quad \frac{A_1}{A_2} = 1.98$$

$$\frac{P_{01}}{P_0} = \frac{P_{01}}{A_1} \cdot \frac{A_1}{A_1^*} = \frac{A_1}{A_1^*} \cdot \frac{A_1}{A_1^*} = 0.8225 \rightarrow P_2 = \frac{P_2}{P_1} \cdot \frac{P_1}{P_1^*} \cdot \frac{P_{01}}{P_1} \cdot P_0 = 232.9 \text{ kPa}$$

Vari. Tot. + LS

$$P_0 = 100 \text{ kPa} \quad \text{Vergleichsraum}$$

$$P_{01} = 0.353 \rightarrow \frac{P_{01}}{P_{02}} = \frac{P_{01}}{P_{02}} = 1.177 \rightarrow P_2 = 250 \text{ kPa} \quad \frac{P_0}{P_{02}} = 0.4 \rightarrow M_0 = 1.22$$

$$\gamma = 4.14$$

$$\left[\frac{G_1}{G_1^*} \cdot \frac{A_1}{A_1^*} = \frac{P_{01}}{P_{01}^*} \right]$$

$$P_0 = 100 \text{ kPa} \quad G_2/G_1 = 1.1$$

Reduktion der P_2 der zu he. Prozessur zu t_1

$$\frac{G_2}{G_1} = \frac{G_2}{G_1} \cdot \frac{G_1}{G_1^*} = 0.558 \rightarrow M_2 = 0.2806 \quad \frac{P_2}{P_1^*} = 2.162 \quad P_2 = 375.2 \text{ kPa} \rightarrow P_0 \text{ mehr strömung}$$

Prozessur zu P_2

$$M_3 = 2.40 \xrightarrow{M_1} M_1 = 0.523 \rightarrow \frac{G_1}{G_1^*} = 0.851 \quad \frac{G_2}{G_1} = \frac{G_2}{G_1} \cdot \frac{G_1}{G_1^*} = 0.936 \xrightarrow{M_1} M_2 = 0.654$$

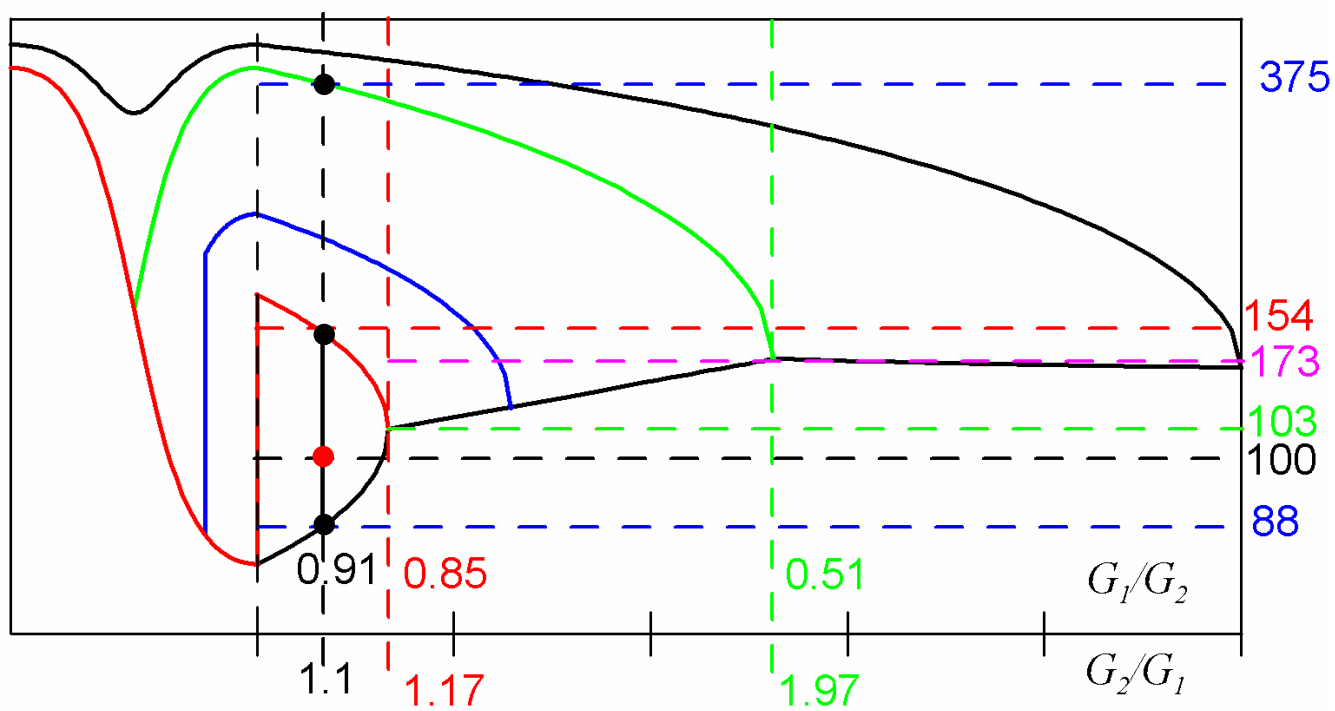
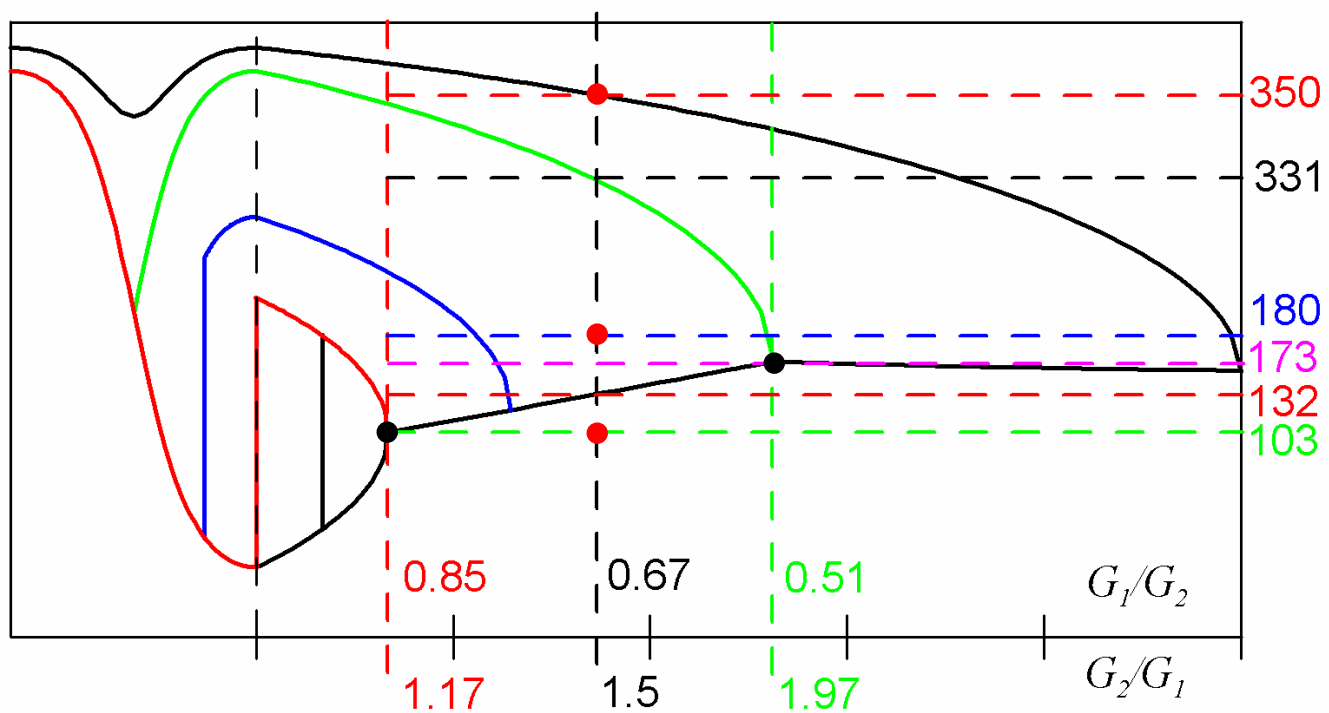
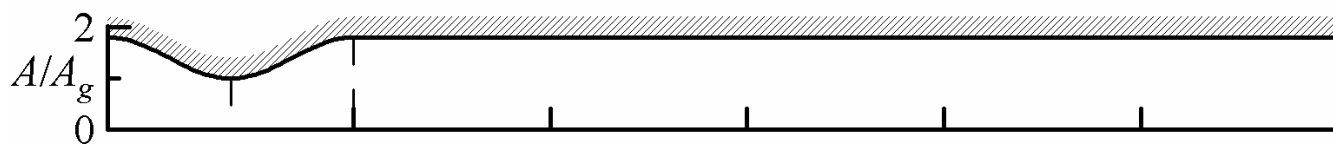
$$\frac{P_{01}}{P_0} = 0.5407 \quad \frac{P_2}{P_1^*} = 1.735 \quad \frac{P_2}{P_{01}^*} = 1.49$$

$$\frac{P_2}{P_{01}} = 0.830 \quad P_2 = \frac{P_2}{P_1^*} \cdot \frac{P_1^*}{P_1} \cdot \frac{P_{01}}{P_1} \cdot P_0 = 154.33 > P_0$$

Prozessur zu t_3

$$\frac{G_2}{G_1} = \frac{G_2}{G_1} \cdot \frac{G_1}{G_1^*} = 0.9362 \rightarrow M_2 = 1.63 \quad \frac{P_2}{P_1^*} = 0.508 \quad P_2 = 52.5 \text{ kPa} < P_0 \rightarrow \text{only d'inter obstruk}$$

$$\frac{P_0}{P_2} = 1.90 \xrightarrow{M_{2, \text{krit}}} M_{2, \text{krit}} = 1.33 \rightarrow M_{2, \text{krit}} = 0.77 \quad E = 0.5 \quad \frac{M_{2, \text{krit}}}{M_2} = 54.4\% \rightarrow$$



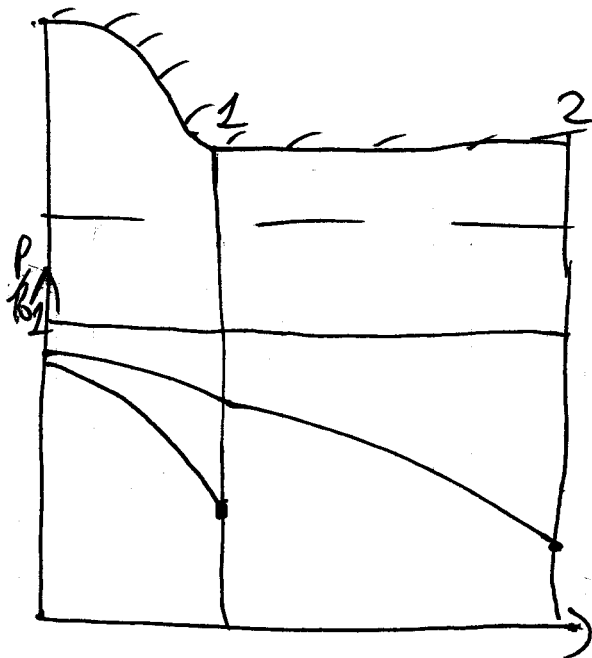
Dati									
gamma	1.4				G2/G*	0.810866			
R	287		Condizioni	1	Condizioni	2			
Po1	1.00E+06	Pa	p/po	0.957453	M	0.477471			
To1	500	K	T/To	0.987654	p/po	0.956393			
M1	0.25		p	9.57E+05	T/To	0.845353			
G2/G1	1.6	%	T	493.8272					
			T/T*	1.185185	T/T*	1.147671			
			p/p*	2.206897	p/p*	1.819325			
			po/po*	1.217672	po/po*	1.123439			
			G/G*	0.506791					
					T2	478.1963			
					p2	7.89E+05			
					po2	9.23E+05			
+++++									
Dati									
gamma	1.4								
R	287				G2/G*	0.216185			
Po1	1.00E+06	Pa	Condizioni	1	Condizioni	2			
To1	500	K	p/po	0.843019	M	0.099955			
M1	0.5		T/To	0.952381	p/po	0.998006			
G2/G1	0.26	%	p	8.43E+05	T/To	0.833887			
			T	476.1905					
			T/T*	1.142857	T/T*	1.197607			
			p/p*	1.777778	p/p*	2.366893			
			po/po*	1.114053	po/po*	1.259153			
			G/G*	0.831479					
					T2	499.0029			
					p2	1.12E+06			
					po2	1.13E+06			
Razzo									
D	0.025								
rpunto	0.025								
rho	2500								
gamma	1.4								
R	320								
T	3000								
L	0.3								
Agola	0.0003								
psistar	0.8101852								
port	1.4726216								
Agrano	0.0004909								
Ag/Agola	1.6362462								
Mgrano	0.3862991								
T/To	1	supponiamo che sia unitario							
To	3000		e,f						
ao	1159.3101		G/G*	0.71045					
po	7024011.8		Ge	3000					
c,d			G*	4222.675					
po/po*	1.1624713		pe/poe	0.90219					
M	0		pe	6336991					
po/po*	1.2678763		deltap	-1323910					
Poin	7660901.8								
rho	7.980106								

Ugello convergente condotto adduzione massa									
Dati									
gamma	1.4								
R	287								
Po1	125	kPa							
To1	350	K							
pa	100	kPa							
G2/G1	1.6	%							
M2	G/G*	p/p*	G1/G*	M1	p/po	p/p*	p2	Err	M2
1	1	1	0.625	0.323759	0.9299583	2.092875	55.54312	-0.44456879	0.8
0.8	0.9818086	1.265823	0.61363	0.316125	0.9330797	2.105431	70.12303	-0.2987697	0.390162
0.390162	0.7152794	1.978374	0.44705	0.216418	0.9678936	2.252313	106.2716	0.06271628	0.461268
0.461268	0.7950417	1.849177	0.496901	0.2443	0.9593201	2.21493	100.1133	0.00113345	0.462576
0.462576	0.7963512	1.846768	0.49772	0.24477	0.9591678	2.214273	99.99673	-3.2739E-05	0.46254
0.46254	0.7963145	1.846836	0.497697	0.244757	0.9591721	2.214292	100	1.2529E-08	0.46254
0.46254	0.7963146	1.846836	0.497697	0.244757	0.9591721	2.214292	100	1.3799E-13	0.46254
0.46254	0.7963146	1.846836	0.497697	0.244757	0.9591721	2.214292	100	-4.2633E-16	0.46254

Ugello convergente-divergente										
Dati										
gamma	1.4									
R	287									
Po1	400									
To1	350									
		kPa								
A/A*	2.4									
Sup		Sub								
M	2.3985993	M	0.250305							
G/G*	0.85112819	G/G*	0.507317							
p/po	0.06854912	p/po	0.957352							
p/p*	0.26505893	p/p*	2.206463							
p*/po	0.2586184	p*/po	0.433885							
p*	103.44736	p*	173.5541							
Dati										
pa	350	kPa								
G2/G1	1.5	G1/G2	0.666667							
Supponedo di passare per r1 si ha							1.217561	1.23459588		
G2/G*	M2	p/p*	p2				1.013991			
0.7609757	0.42900946	1.908293	331.192	minore pa moto non strozzato						
M2	G/G*	p/p*	G1/G*	M1	p/po	p/p*	p2	Err	M2	
0.4290095	0.76097566	1.908293	0.507317	0.250305	0.9573519	2.206463	331.192	-0.0537371	0.2	
0.2	0.41659779	2.272727	0.277732	0.129527	0.988344	2.344922	383.1661	0.0947602	0.346137	
0.3461372	0.6571529	2.05526	0.438102	0.211549	0.9692935	2.258495	352.8279	0.00807967	0.359759	
0.3597589	0.67586389	2.031837	0.450576	0.218347	0.9673308	2.249833	349.4407	-0.0015979	0.35751	
0.3575098	0.67281941	2.035729	0.448546	0.217236	0.9676555	2.251263	350.0052	1.4914E-05	0.357531	
0.3575306	0.67284765	2.035694	0.448565	0.217246	0.9676525	2.25125	350	2.65E-08	0.357531	
0.3575307	0.6728477	2.035693	0.448565	0.217246	0.9676525	2.25125	350	-4.429E-13	0.357531	
0.3575307	0.6728477	2.035693	0.448565	0.217246	0.9676525	2.25125	350	-1.624E-16	0.357531	
Dati										
pa	180	kPa								
G2/G1	1.5	G1/G2	0.666667							
Supponedo di passare per r1 si ha										
G2/G*	M2	p/p*	p2							
0.7609757	0.42900946	1.908293	331.192	maggiore pa moto strozzato						
Supponendo M2 =1 ond d'urto										
M2	G1/G*	M1	p/po	A/A*	po1/po	p/p*	p2			
1	0.66666667	0.353004	0.917448	1.76502	0.7354249	2.043498	132.0704	< pa ond d'urto		

M2	G/G*	p/p*	G1/G*	M1	p/po	A/A*	po1/po	p/p*	p2	Err	M2
1	1	1	0.666667	0.353004	0.9174483	1.76502	0.735425	2.04349839	132.0704	-0.266275295	0.6
0.6	0.90494342	1.595745	0.603296	0.309301	0.9358177	1.980467	0.825194	2.11652471	232.8883	0.29382376	0.809837
0.809837	0.983772	1.251192	0.655848	0.345205	0.9208687	1.79915	0.749646	2.05685016	167.9714	-0.066825739	0.770956
0.7709557	0.97518364	1.309957	0.650122	0.341138	0.9226281	1.817621	0.757342	2.06376127	177.4092	-0.014393333	0.760282
0.7602823	0.9724214	1.326523	0.648281	0.339839	0.9231867	1.823623	0.759843	2.06596172	180.1632	0.000906414	0.760915
0.7609147	0.97259016	1.325537	0.648393	0.339918	0.9231527	1.823256	0.75969	2.06582759	179.9979	-1.1571E-05	0.760907
0.7609067	0.97258803	1.325549	0.648392	0.339917	0.9231531	1.82326	0.759692	2.06582928	180	-9.18734E-09	0.760907
0.7609067	0.97258803	1.325549	0.648392	0.339917	0.9231531	1.82326	0.759692	2.06582928	180	9.34758E-14	0.760907
Dati											
pa	100	kPa									
G2/G1	1.5	G1/G2	0.666667								
Supponedo di passare per r1 si ha											
G2/G*	M2	p/p*	p2								
0.7609757	0.42900946	1.908293	331.192	maggiore pa moto strozzato							
Supponendo M2 =1											
M2	G1/G*	M1	p/po	A/A*	po1/po	p/p*	p2		po1/po2=po1/po*		
1	0.66666667	0.353004	0.917448	1.76502	0.7354249	2.043498	132.0704	>pa ventaglio	1.17668		
po2	pa/po2	Ma	ni								
250	0.4	1.22324	4.139316		1.1766799						
Dati											
pa	100	kPa									
G2/G1	1.1	G1/G2	0.909091								
Supponedo di passare per r1 si ha											
G2/G*	M2	p/p*	p2								
0.5580488	0.28058765	2.161731	375.1773	maggiore pa moto strozzato							
Supponedo di passare per r2 si ha											
M1	po1/po	G/G*	p/po1	p/p*	G2/G*	M2	p/p*	p2			
0.5232674	0.54073497	0.851128	0.829774	1.734941	0.936241	0.659375	1.491902	154.333308			
Supponedo di passare per r3 si ha											
G2/G*	M2	p/p*	p2								
0.936241	1.63084045	0.508098	52.56141	minore pa onda d'urto obliqua							
pa/p2	Mn2	Mnv	eps								
1.9025364	1.33176673	0.770314	54.74724								

Moto con espansione di Masse



$$\gamma = 1.4 \quad R = 287 \frac{\text{J}}{\text{kg} \cdot \text{K}} \quad P_2 = 70 \times P_0 \quad P_0 = 100 \times P_2$$

$$D_1 = D_2 = 0.05 \text{ m} \quad T_0 = 350 \text{ K}$$

Considerando solo l'ugello
Per moto stazionario v. ho:

$$\dot{m} = \frac{P_0 A_1 \Psi^+}{\alpha_0} \Rightarrow G_u^* = \frac{\dot{m}}{A_1} = \frac{P_0 \Psi^+}{\alpha_0} =$$

$$G_u^* = \frac{100 \cdot 0.81 \cdot 10^3}{\sqrt{1.4 \cdot 287 \cdot 350}} = 0.216 \frac{\text{kg}}{\text{m}^2 \text{s}}$$

Supponiamo che la massa aggiunta
sia il 20% di G_u^*

$$\Delta G = G_u^* \cdot 0.2 = 0.0432 \frac{\text{kg}}{\text{m}^2 \text{s}}$$

Si procede per tentativi. Supponiamo $M_1 = 0.2$

$$M_1 = 0.2 \xrightarrow{M_1} P_1/P_0 = 2.27$$

$$\downarrow 150 \quad G_1 = 0.417$$

$$\frac{P_1}{P_0} = 0.973$$

$$\frac{A_1}{A^*} = 2.96 \rightarrow G_1 = G_u^* \frac{A_1^*}{A_1} = \frac{0.216}{2.96} = 0.0729 \frac{\text{kg}}{\text{m}^2 \text{s}} \quad \Delta G = 0.593$$

$$\frac{G_2}{G_1} = \frac{\Delta G + G_1}{G_1} = 1 + \frac{\Delta G}{G_1} = 1.593 \rightarrow \frac{G_2}{G_1^*} = \frac{G_2}{G_1} \frac{G_1}{G_1^*} = 1.59 \cdot 0.417 = 0.664$$

$$\frac{G_2}{G_1^*} = 0.664 \xrightarrow{M_2} M_2 = 0.351$$

$$\frac{P_2}{P_1} = 2.05$$

$$P_2 = \frac{P_2}{P_1} \frac{P_1}{P_0} = \frac{2.05}{2.27} \cdot 100 = 87.6$$

$$M_1 = 0.25 \xrightarrow{M_1} P_1/P_0 = 2.21 \quad G_1/G_1^* = 0.507$$

$$\downarrow 150$$

$$\frac{P_1}{P_0} = 0.973 \quad \frac{A_1}{A^*} = 2.40 \quad G_1 = 0.0899 \quad \frac{\Delta G}{G_1} = 0.481$$

$$\frac{G_2}{G_1} = 1.48 \quad \frac{G_2}{G_1^*} = 0.750 \xrightarrow{M_2} M_2 = 0.420 \quad P_2 = 83.56$$

$$\frac{P_2}{P_1} = 1.43$$

Verif. Tab.

S₂ e Suppore $M_2 = 0.4 \rightarrow \frac{P_2}{P_1} = 1.96$

$$\frac{G_2}{G^*} = 0.727$$

S₁ Suppore $G_1 = Q \cdot G_2^*$ con $Q = 0.3$ $\frac{G_2}{G_1} = \frac{0.0432}{0.3 \cdot 0.28} = 0.517$

$\frac{G_2}{G_1} = 1.67$ $\frac{G_1}{G_2} = \frac{G_1}{G_2} \cdot \frac{G_2}{G_1} = \frac{0.727}{1.67} = 0.435 \xrightarrow{M_2} M_1 = 0.21 \rightarrow \frac{P_1}{P_2} = 0.970$
 $\frac{P_1}{P_2} = 2.26$ $\frac{A_2}{A_1} = 2.82$

$G_1 = G_2^* \frac{A_1}{A_2} = \frac{0.216}{2.82} = 0.0766 \frac{kg}{m^2 s}$ $Q = \frac{G_1}{G_2^*} = \frac{A_1}{A_2} = \frac{1}{2.82} = 0.354$

S₁ itera con $Q = 0.4$ (Verli Tab)

Dopo 3 iterazioni si trova $Q = 0.395$ e $M_1 = 0.236$ $\frac{P_1}{P_2} = 0.982$
 $\frac{P_1}{P_2} = 2.13$

Altro iterazione con $M_2 = 0.3$

$P_0 = 99.4$

$P_2 = 84.7$

Verli Tab

gamma	1.4			pa	70	kPa											
R	287			G* ugello	0.216												
Po1	100	kPa		perc DG	20%												
To1	350	K		DeltaG	0.0432												
D	0.05	m		A1	0.00196												
M1	p1/p*	G1/G*	p1/p01	Au/A*	G1	DG/G1	G2/G1	G2/G*	M2	p2/p*	p2	Err					
0.2	2.27273	0.4166	0.9725	2.96352	0.07289	0.5927	1.5927	0.66352	0.35072	2.04743	87.609	17.609	0.25				
0.25	2.2069	0.50679	0.95745	2.40271	0.0899	0.48054	1.48054	0.75033	0.41955	1.9255	83.5368	13.5368	0.41621				
0.41621	1.93155	0.74649	0.88762	1.53999	0.14026	0.308	1.308	0.97641	0.77593	1.30229	59.8454	-10.155	0.34497				
0.34497	2.05725	0.65552	0.92097	1.8002	0.11998	0.36004	1.36004	0.89153	0.57858	1.63414	73.1557	3.15565	0.36186				
0.36186	2.02819	0.67869	0.91349	1.72821	0.12498	0.34564	1.34564	0.91328	0.61435	1.57028	70.7248	0.72483	0.3669				
0.3669	2.01942	0.68541	0.91121	1.70815	0.12645	0.34163	1.34163	0.91956	0.6258	1.55012	69.9448	-0.0552	0.36654				
0.36654	2.02005	0.68494	0.91137	1.70955	0.12635	0.34191	1.34191	0.91912	0.62497	1.55156	70.0009	0.00095	0.36655				
0.36655	2.02003	0.68494	0.91137	1.70953	0.12635	0.34191	1.34191	0.91913	0.62499	1.55154	70	1.2E-06	0.36655				
0.36655	2.02003	0.68494	0.91137	1.70953	0.12635	0.34191	1.34191	0.91913	0.62499	1.55154	70	-3E-11	0.36655				
0.36655	2.02003	0.68494	0.91137	1.70953	0.12635	0.34191	1.34191	0.91913	0.62499	1.55154	70	0	0.36655				
M2	p2/p*	G2/G*	%G1	DG/G1	G2/G1	G1/G*	M1	p1/p*	p1/p01	Au/A*	G1	%G1	Err	%G1	p2	Err	M1
0.4	1.96078	0.72734	0.3	0.66667	1.66667	0.43641	0.21063	2.25965	0.96955	2.82127	0.07656	0.35445	0.05445	0.35			
0.4	1.96078	0.72734	0.35	0.57143	1.57143	0.46285	0.22511	2.24101	0.96532	2.64968	0.08152	0.3774	0.0274	0.40066			
0.4	1.96078	0.72734	0.40066	0.49917	1.49917	0.48516	0.23761	2.22419	0.96146	2.51895	0.08575	0.39699	-0.0037	0.39468			
0.4	1.96078	0.72734	0.39468	0.50674	1.50674	0.48273	0.23623	2.22608	0.9619	2.53267	0.08528	0.39484	0.00016	0.39493	84.7262	14.7262	0.3
0.3	2.13144	0.58895	0.39493	0.50642	1.50642	0.39096	0.18649	2.28857	0.97603	3.16835	0.06817	0.31562	-0.0793	0.39468			
0.3	2.13144	0.58895	0.39468	0.50674	1.50674	0.39088	0.18645	2.28862	0.97604	3.16907	0.06816	0.31555	-0.0791	0.28449			
0.3	2.13144	0.58895	0.28449	0.703	1.703	0.34583	0.16331	2.31362	0.98155	3.60066	0.05999	0.27773	-0.0068	0.27419			
0.3	2.13144	0.58895	0.27419	0.72942	1.72942	0.34055	0.16064	2.31632	0.98214	3.65857	0.05904	0.27333	-0.0009	0.27269	90.3753	20.3753	0.66068
0.66068	1.48967	0.93684	0.27269	0.73343	1.73343	0.54045	0.26988	2.17792	0.95064	2.23941	0.09645	0.44655	0.17386	0.27418			
0.66068	1.48967	0.93684	0.27418	0.72944	1.72944	0.5417	0.27063	2.1768	0.95038	2.23372	0.0967	0.44768	0.1735	1.00134			
0.66068	1.48967	0.93684	1.00134	0.19973	1.19973	0.78087	0.44745	1.87457	0.87161	1.45501	0.14845	0.68728	-0.3141	0.53295			
0.66068	1.48967	0.93684	0.53295	0.37527	1.37527	0.6812	0.36373	2.02493	0.91265	1.72067	0.12553	0.58117	0.04822	0.59529	67.1399	-2.8601	0.61628
0.61628	1.56686	0.91436	0.59529	0.33597	1.33597	0.68442	0.36615	2.02073	0.91155	1.71109	0.12623	0.58442	-0.0109	0.58383			
0.61628	1.56686	0.91436	0.58383	0.34257	1.34257	0.68105	0.36362	2.02513	0.9127	1.72112	0.1255	0.58102	-0.0028	0.57983			
0.61628	1.56686	0.91436	0.57983	0.34493	1.34493	0.67986	0.36273	2.02668	0.9131	1.7247	0.12524	0.57981	-2E-05	0.5798			
0.61628	1.56686	0.91436	0.5798	0.34495	1.34495	0.67985	0.36272	2.02669	0.9131	1.72473	0.12523	0.5798	-4E-08	0.5798	70.593	0.59302	0.62391
0.62391	1.55343	0.91855	0.5798	0.34495	1.34495	0.68296	0.36506	2.02263	0.91205	1.71541	0.12591	0.58295	0.00315	0.5798			
0.62391	1.55343	0.91855	0.5798	0.34495	1.34495	0.68296	0.36506	2.02263	0.91205	1.71541	0.12591	0.58295	0.00315	0.58434			
0.62391	1.55343	0.91855	0.58434	0.34227	1.34227	0.68433	0.36608	2.02085	0.91158	1.71136	0.12621	0.58433	-7E-06	0.58433			
0.62391	1.55343	0.91855	0.58433	0.34227	1.34227	0.68432	0.36608	2.02085	0.91158	1.71137	0.12621	0.58433	1.6E-08	0.58433	70.0735	0.0735	0.62499
0.62499	1.55154	0.91913	0.58433	0.34227	1.34227	0.68476	0.3664	2.02028	0.91143	1.71008	0.12631	0.58477	0.00044	0.58433			
0.62499	1.55154	0.91913	0.58433	0.34227	1.34227	0.68476	0.3664	2.02028	0.91143	1.71008	0.12631	0.58477	0.00044	0.58496			
0.62499	1.55154	0.91913	0.58496	0.34191	1.34191	0.68494	0.36655	2.02003	0.91137	1.70953	0.12635	0.58496	-1E-07	0.58496			
0.62499	1.55154	0.91913	0.58496	0.34191	1.34191	0.68494	0.36655	2.02003	0.91137	1.70953	0.12635	0.58496	4.3E-11	0.58496	70	-1E-05	0.62499