



# On plasma vertical stabilization at EAST tokamak

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## Outline



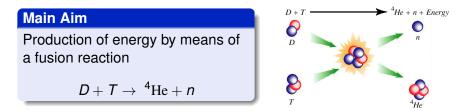
- The plasma vertical stabilization problem
- 2 Plasma-circuits linearized model
- Vertical stabilization at EAST with a SISO controller
- Vertical stabilization at EAST with a MIMO controller





Introduction

## **Nuclear Fusion for Dummies**



#### Plasma

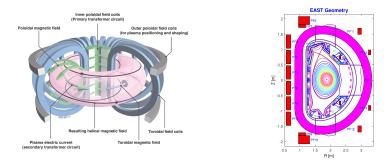
- High temperature and pressure are needed
- Fully ionised gas  $\mapsto$  Plasma
- Magnetic field is needed to confine the plasma





Introduction

#### **Plasma magnetic control**



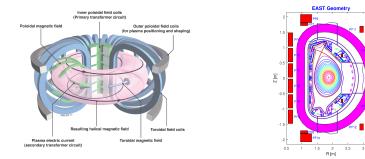
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Introduction

#### **Plasma magnetic control**



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- In order to obtain good performance, it is necessary to have a plasma with vertically elongated cross section ⇒ vertically unstable plasmas



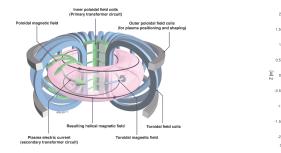


EAST Geometry

1.5

Introduction

#### **Plasma magnetic control**



- In tokamaks, magnetic control of the plasma is obtained by means of magnetic fields produced by the external active coils
  - In order to obtain good performance, it is necessary to have a plasma with vertically elongated cross section ⇒ vertically unstable plasmas
  - It is important to maintain adequate plasma-wall clearance during operation

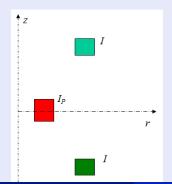




## The plasma vertical instability

#### Simplified filamentary model

Consider the simplified electromechanical model with three conductive rings, two rings are kept fixed and in symmetric position with respect to the r axis, while the third can freely move vertically.



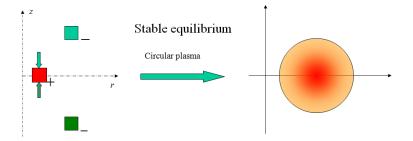
If the currents in the two fixed rings are equal, the vertical position z = 0 is an equilibrium point for the system.





# Stable equilibrium - 1/2

If  $sgn(I_p) \neq sgn(I)$ 

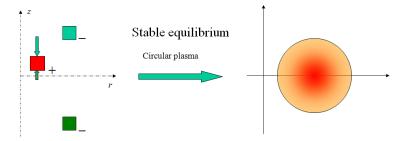






# Stable equilibrium - 2/2

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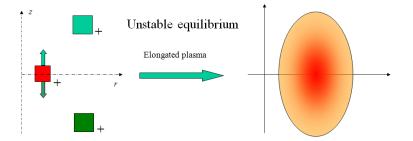






# Unstable equilibrium - 1/2

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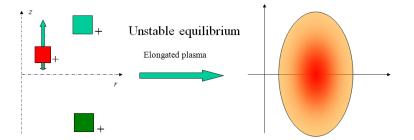






#### Unstable equilibrium - 2/2

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## Vertical stabilization problem

 The plasma vertical instability reveals itself in the linearized model by the presence of an unstable eigenvalue in the dynamic system matrix



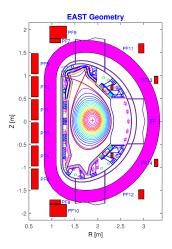


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#### Objectives

- The VS is the essential magnetic control system!
- Vertically stabilize elongated plasmas in order to avoid disruptions
- Counteract the effect of disturbances
- It does not necessarily control vertical position but it *simply* stabilizes the plasma







Plasma linearized model

# **Plasma-circuits linearized model**

Starting from the nonlinear lumped parameters model, the following plasma linearized state space model can be easily obtained:

$$\delta \dot{\mathbf{x}}(t) = \mathbf{A} \delta \mathbf{x}(t) + \mathbf{B} \delta \mathbf{u}(t) + \mathbf{E} \delta \dot{\mathbf{w}}(t), \tag{1}$$

$$\delta \mathbf{y}(t) = \mathbf{C} \,\,\delta \mathbf{I}_{PF}(t) + \mathbf{F} \delta \mathbf{w}(t), \tag{2}$$

where:

- A, B, E, C and F are the model matrices
- $\delta \mathbf{x}(t) = \left[ \delta \mathbf{I}_{PF}^{T}(t) \ \delta \mathbf{I}_{e}^{T}(t) \ \delta I_{p}(t) \right]^{T}$  is the state space vector
- $\delta \mathbf{u}(t) = \left[ \delta \mathbf{U}_{PF}^{T}(t) \mathbf{0}^{T} \mathbf{0} \right]^{T}$  are the input voltages variations
- $\delta \mathbf{w}(t) = \left[\delta \beta_{p}(t) \, \delta I_{i}(t)\right]^{T}$  are the  $\beta_{p}$  and  $I_{i}$  variations
- $\delta \mathbf{y}(t)$  are the output variations

The model (1)–(2) relates the variations of the PF currents to the variations of the outputs around a given equilibrium





# Stabilizing the EAST plasma using a SISO controller - 1/2

$$\Sigma : \begin{cases} \dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t) + \mathbf{B}\mathbf{u}(t), & \mathbf{x}(0) = \mathbf{x}_0 \\ \mathbf{y}(t) = \mathbf{C}\mathbf{x}(t) \end{cases}$$

• From  $\Sigma$  it is possible to derive the input-output relationship between the vertical speed  $V_p(s)$  and the voltage applied to the in-vessel coil  $U_{IC}(s)$  (the plasma)

$$W_{
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• From  $\Sigma$  it is possible to derive the input-output relationship between the vertical speed  $V_{\rho}(s)$  and the voltage applied to the in-vessel coil  $U_{IC}(s)$  (the plasma)

$$W_{p}(s) = rac{V_{p}(s)}{U_{lC}(s)}$$

• The IC power supply is modeled as

$$U_{\mathit{IC}}(s) = rac{e^{-\delta_{\mathit{PS}}s}}{1+s au_{\mathit{PS}}} \cdot U_{\mathit{IC}_{\mathit{ref}}}(s) \, ,$$

with  $U_{lC_{ref}}(s)$  the voltage requested by the controller,  $\delta_{\rho s} = 550 \ \mu s, \tau_{\rho s} = 100 \ \mu s$ 





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 At EAST the plasma vertical speed V<sub>ρ</sub>(s) is estimated by means of a derivative filter applied on Z<sub>ρ</sub>(s), i.e.

$$V_{\mathcal{P}}(s) = rac{s}{1+s au_{\mathcal{V}}} \cdot Z_{\mathcal{P}}(s) \, ,$$

with  $\tau_v = 1$  ms.





#### Stabilizing the EAST plasma using a SISO controller - 2/2

• Putting everything together we get

$$\mathcal{W}_{\mathit{plant}}(s) = rac{s}{(1+s au_{\mathit{ps}})} \cdot \mathcal{W}_{\mathit{p}}(s) \cdot e^{-\delta_{\mathit{ps}}s}\,,$$





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• The 550  $\mu$ s time delay of the IC power supply can be replaced by its third order Padé approximation

$$\frac{-(s-8444)(s^2-1.34\cdot 10^4s+8.54\cdot 10^7)}{(s+8444)(s^2+1.34\cdot 10^4s+8.54\cdot 10^7)}$$





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 The only way to vertically stabilize EAST with a SISO stable controller (SISO strong stabilizability) is to include an integral action on the vertical speed (i.e., the vertical position z<sub>p</sub> should be fed back





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Stabilizing EAST with a SISO controller

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- The only way to vertically stabilize EAST with a SISO stable controller (SISO strong stabilizability) is to include an integral action on the vertical speed (i.e., the vertical position z<sub>p</sub> should be fed back
- The reason is that the plasma unstable pole is *trapped* between two non minimum phase zeros





Parity-Interlacing-Property (PIP)

#### Theorem

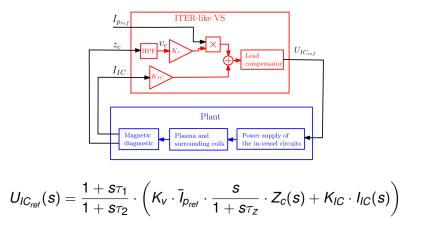
A linear plant W(s) is strongly stabilizable if and only if the number of poles of W(s) between any pair of real zeros in the right-half-plane (RHP) is even.

D. C. Youla, J. J. Bongiorno Jr., C. N. Lu Single-loop feedback stabilization of linear multivariable dynamical plants *Automatica*, vol. 10, no. 2, pp. 159–173, Mar. 1974





#### Stabilizing with a MIMO controller - 1/3

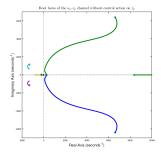




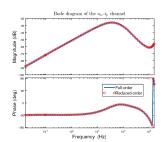


#### Stabilizing with a MIMO controller - 2/3

By closing the loop on  $I_{lC}(s)$  we introduce another unstable pole in the  $u_{ic} - \dot{z}_{p}$  channel



(a) Root locus of the  $u_{ic} - \dot{z}_{\rho}$  channel, when the loop on the IC current is closed.



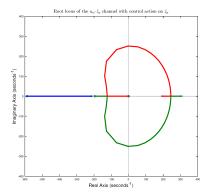
(b) Bode diagrams of the fullorder and reduced-order versions of transfer function for the  $u_{ic} - \dot{z}_p$ channel, when the loop on the IC current is closed.





#### Stabilizing with a MIMO controller - 3/3

Closing a stable controller on the vertical speed is now possible to stabilize the EAST plasma



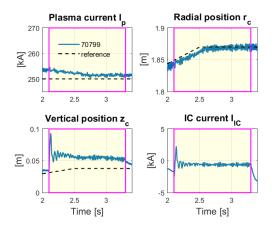
**Figure :** Root locus of the  $u_{ic} - \dot{z}_p$  channel, when the loop on the IC current is also closed.

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#### **Experimental results - Dec 2016**



**Figure :** EAST pulse #70799. During this pulse the *ITER-like* VS was enabled from t = 2.1 s for 1.2 s, and only  $I_p$  and  $r_c$  were controlled, while  $z_c$  was left uncontrolled. This first test confirmed that the ITER-like VS vertically stabilized the plasma by controlling  $\dot{z}_c$  and  $I_{IC}$ , without the need to feed back the vertical position  $z_c$ .

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#### Conclusions

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Thank you!