Previous Experience & Proposal for Future Work

Gianmaria DE TOMMASI – CREATE/Università di Napoli Federico II – Italy Email: detommas@unina.it Thanks to Marcello Cinque, Sara Dubbioso, Federico Fiorenza and Daniele Ottaviano

Plasma Control ISFN Meeting - ITER HQ, 23 Sep 2025





Background & main topics



My background

2001 MSc in Electronic Engineering in 2001 - University of Naples Federico II

2002-2005 PhD in Control Engineering - University of Naples Federico II (. . . and at JET with the PPCC group)

2002-... Member of the CREATE Consortium (research grants & contracts for JET, EAST, JT-60SA, DTT,

2009-. . . Various contracts with ITER (Central Safety System, Central Interlock System, Plasma Control System)



Topics

- Development of real-time software framework for fusion devices
- 2 Design and deployment of plasma (magnetic) control systems
- 3 System-engineering approach for PCS design



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- 1 RT software frameworks Past experience (very long ago)
- 2 RT Frameworks Recent & possible future works
- 3 Plasma control Past experience
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- 5 System-engineering: the ITER experience & possible future works

JETRT

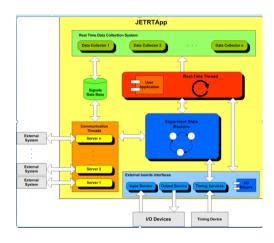


- The JETRT framework was developed in 2002/2003 to deploy the eXtreme Shape Controller (XSC)
- JETRT was based on the cross-platform BaseLib library (developed by the JET PPCC group)



G De Tommasi et al

A flexible software for real-time control in nuclear fusion experiments *Contr. Eng. Prac.*, 2006

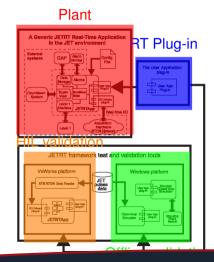


Real-time application plug-in



The Real-time Application Plug-in that can be used to:

- perform offline validation against a plant model
- perform real-time validation with hardware-in-the-loop
- run the real-time system on the plant



MARTe - The origins (2004-2005)





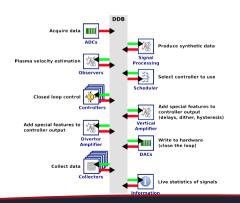
MARTe real-time thread for the JET VS5



A. C. Neto et al.

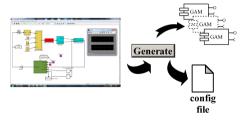
MARTe: A Multiplatform Real-Time Framework

IEEE Trans. Nucl. Sci., 2010



Automatic code (& configuration) generation





- Commonly used in many fields: rapid prototyping (dSpace, NI, Mathworks,...), automotive, railway, ...
- Included in most of the RTFs for fusion devices (TCV RTF, ITER RTF, MARTe2+MDSplus)

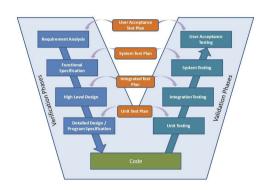
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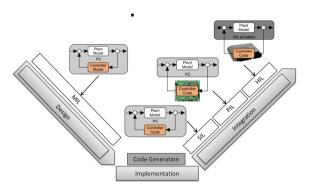


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x-in-the-loop V&V

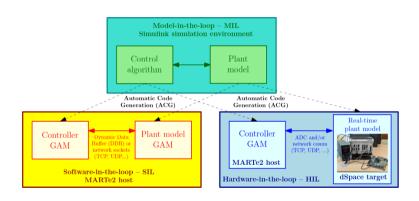






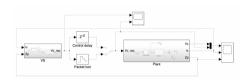
Setup for *x*-in-the-loop V&V





Example: the DTT VS system



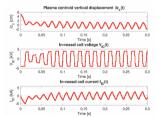




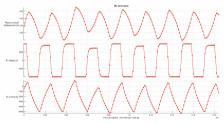
S. Dubbioso et al.

Rapid prototyping of control modules for the DTT Plasma Control System

Fus. Eng. Des., 2025



MIL simulation of a 5 cm VDE rejection with a systematic packet loss rate equal to $N_{\text{max}}^{MIL} = 89\%$; transmission frequency is assumed equal to 1 kHz.

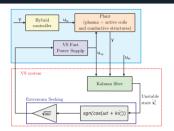


HIL simulation (SCALEXIO) of a 5 cm VDE in presence of a systematic packet loss set equal to $N_{max}^{HIL} = 91\%$.

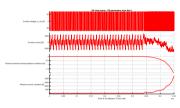


Example: a Extremum-seeking based VS

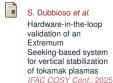


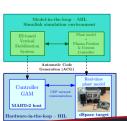


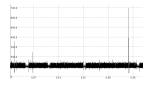
Functional architecture ES-based VS for TCV



Time traces recorded during HIL simulation. Vertical stability is lost when a delay of about 600 μs is introduced in the control loop.





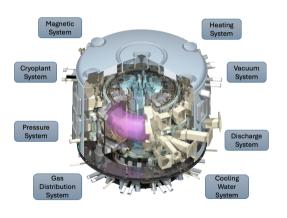


VS thread execution time (measured in μs) during the HIL simulation



Control hw/sw isolation





- Can we use cloud technologies in the context of ITER to consolidate multiple isolated control systems on the same hardware?
- Possible objectives
 - Fast prototyping
 - Cost reduction
 - Heterogeneous spread redundancy
 - Diversified control & protection systems

Contributions

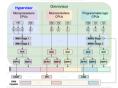


- Real-time containers
 - Use the same abstraction everywhere
 - Ensuring temporal isolation
 - Containers on co-kernels (RTAI, Xenomai)
 - Containers on partitioning hypervisors (Jailhouse)
 - Containers on MPSoCs (on RPU/FPGA via the Omnivisor)
- Memory and I/O isolation
 - Reducing/controlling memory interference from co-accessing cores
 - Real-time I/O access regulation
- Criticality-aware orchestration
 - Placement & monitoring driven by containers criticality and the isolation assured by nodes (K4.0s)
 - Temporal isolation assessment
 - Placement prioritization (Preempt-K8s)

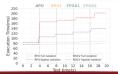
rt-containers on co-kernels



Ominvisor

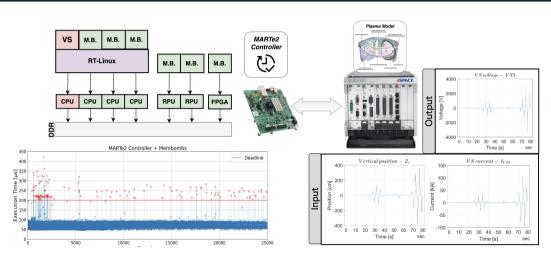


Isolation results on MPSoCs



HIL simulation of VS with co-located interference







Isolation with rt-container and omnivisor







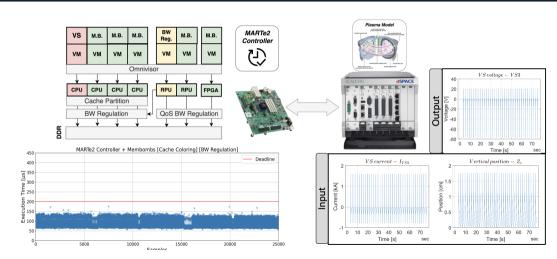


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eXtreme Shape Controller



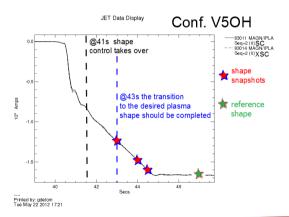
- Design & implementation of the eXtreme Shape Controller (XSC)
- MIMO approach for plasma shape control
- It minimizes the steady-state MSE over a number of plasma shape descriptor that is greater than the number of actuators
- Exploits the SVD of a linear relationship between the PF currents and the controlled paramters
- Model-based approach that (partially) trades robustness for performance
- Originally implemented at JET but tested also on other machines (EAST, ...)



Plasma Shape Control at JET during I_p ramp-up



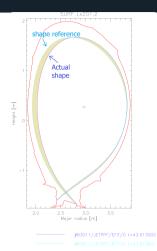
- #83011 plasma ramp-up with standard JET SC
- #83014 plasma ramp-up with XSC

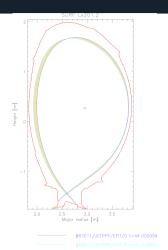


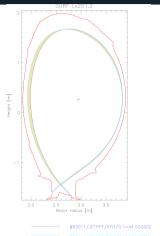


#83011 - Shape tracking during the ramp-up with SC









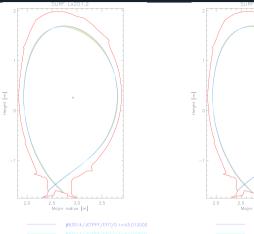
@43s

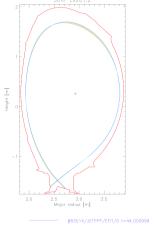
@44s

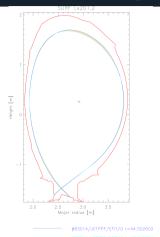
@44.5s

#83014 - Shape tracking during the ramp-up with XSC









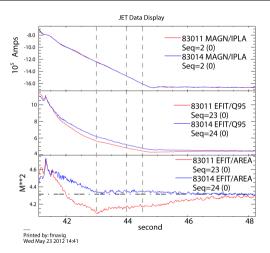
@43s

@44s

@44.5s

Plasma surface and q95

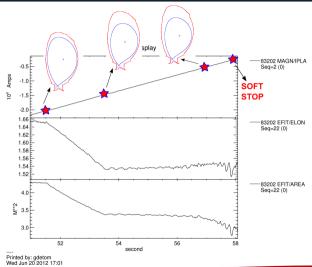






Change of elongation during the plasma current ramp-down



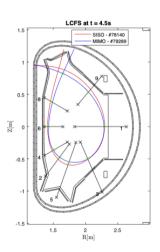




Isoflux XSC at EAST



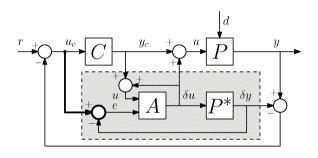
- Comparison between the SISO and MIMO shape controllers (pulses #78140 and #79289)
- The LCFS at t = 4.5 s is shown together with the control points and the target X-point position





Block diagram of the allocated closed-loop





$$P^* := \lim_{s \to 0} P(s)$$
,

The current allocator block



The current allocator

The allocator equations are given by

$$\dot{x}_{a} = -KB_{0}^{T} \begin{bmatrix} I \\ P^{\star} \end{bmatrix}^{T} (\nabla J)^{T} \Big|_{(u,\delta y)}, \tag{1a}$$

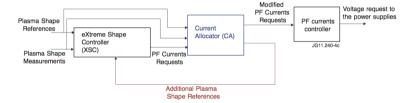
$$\delta u = B_0 x_a, \tag{1b}$$

$$\delta y = P^* B_0 x_a. \tag{1c}$$

- $K \in \mathbb{R}^{n_a \times n_a}$ is a symmetric positive definite matrix used to specify the allocator convergence speed, and to distribute the allocation effort in the different directions
- $J(u^*, \delta y^*)$ is a continuously differentiable cost function that measures the trade-off between the current saturations and the control error (on the plasma shape)
- $B_0 \in \mathbb{R}^{n_{PF} \times n_a}$ is a suitable full column rank matrix

The CLA Architecture

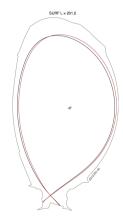




The CLA block is inserted between the XSC and the Current Decoupling Controller

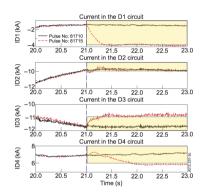
Experimental results of CLA @ JET





Shape comparison at 22.5 s. Black shape (#81710 without CLA), red shape (#81715

with CLA)

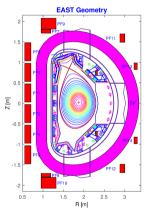


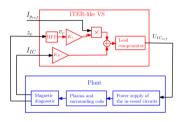
Currents in the divertor circuits. #81710 (reference pulse without CLA) and pulse #81715 (with CLA). The shared areas correspond to regions beyond the current limits enforced by the CLA parameters.



ITER-like VS for the EAST tokamak



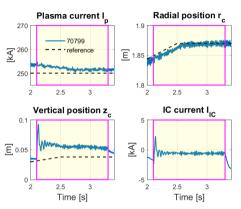




$$U_{\mathit{IC}_{\mathit{ref}}}(s) = rac{1 + s au_1}{1 + s au_2} \cdot \left(extstyle \mathcal{K}_{\mathit{V}} \cdot ar{\mathit{I}}_{\mathit{p}_{\mathit{ref}}} \cdot rac{s}{1 + s au_{\mathit{Z}}} \cdot \mathit{Z}_{\mathit{c}}(s) + \mathcal{K}_{\mathit{IC}} \cdot \mathit{I}_{\mathit{IC}}(s)
ight)$$

Experimental results





EAST pulse #70799. During this pulse the *ITER-like* VS was enabled from t = 2.1 s for 1.2 s, and only I_p and r_c were controlled, while z_c was left uncontrolled. This first test confirmed that the ITER-like VS vertically stabilized the plasma by controlling \dot{z}_c and I_{IC} , without the need to feed back the vertical position z_c

The ITER Magnetic Control Architecture (for PFPO-1/SRO)



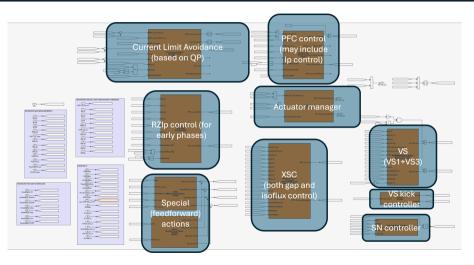


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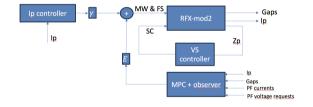


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RFX-mod2 magnetic control with MPC



- The VS controller stabilizes the plasma with the dedicated Saddle Coils
- I_p controller and the MPC for the shape control act on Magnetizing Windings (MW) and Field Shaping (FS) coils (actuator sharing → model-based geometric decoupling)
 - The I_p controller is a PID that acts on a control direction γ that does minimizes the effect on the plasma shape
 - The MPC for the shape control acts along the *subspace* E, where $\gamma^T E = 0$
 - MPC used to not violate voltage limits



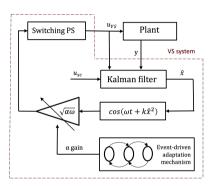
Model-free control with Extremum Seeking



 Control approach based on the minimization (via Extremum Seeking) of a candidate Lyapunov function V(x)

$$u(t) = \omega \cos(\omega t + kV(x))$$

- A Kalman filter is needed to estimate the plasma movement along the unstable mode \hat{x}
- Robustness against such Kalman filter has been observed in simulation
- Kalman filter can be replaced by a NN (trained against simulation data)
- Plan to test it on TCV (still WIP)





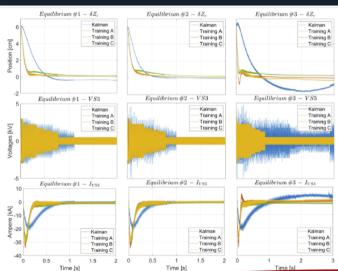
S. Dubbioso et al.

Model-free Stabilization via Extremum Seeking using a cost neural estimator

Expert Sys. Appl., 2024

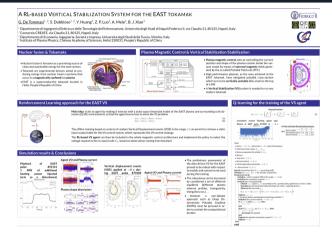
ITER benchmark





RL magnetic control





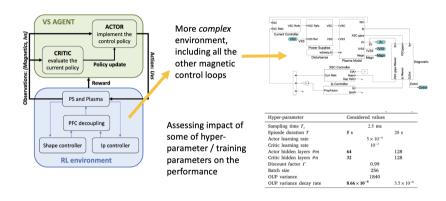


G. De Tommasi et al.

A RL-based Vertical Stabilization System for the EAST tokamak

From naïve Q-learning to DDPG...







S. Dubbioso et al.

A Deep Reinforcement Learning approach for Vertical Stabilization of tokamak plasmas Fus. Eng. Des., 2023



My view (on AI for control...)



- Time & resource consuming activity
- A lot of trial & error
- Need to setup joint activities with big player
 - EPFL/SPC & DeepMind
 - CEA & Capgemini
- Are Al controller really outperforming model-based (adaptive control)?
- Are tokamak discharge so *unpredictable* (once the scenario is assessed)?
 - In the past we trade robustness to some degree to achieve tight control
- What if the AI controller does not work? How to re-tune it (in due time)?
- Al & ML can be beneficial in many other ways...

Fast plasma boundary reconstruction with PIELM



- Physics Informed Neural Networks (PINNs) can be used to solve Partial Differential Equations with initial/boundary conditions.
- PINNs may require long training times
- Given the magnetic measurements m_{ψ} and m_{B} , by solving $\Delta^{*}\psi(r,z)=0$ it is possible to find the LCFS
- This equation can be solved in real-time by Physics-Informed Extreme Learning Machines (PIELMs)



Extreme Learning Machine (ELM)

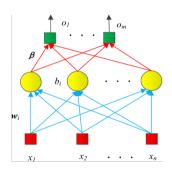


- ELMs are similar to one-layer feedforward NNs and proved to have great generalization capabilities
- The structure of an ELM is the following

$$\psi_{\mathsf{ELM}}(\mathsf{X}) = \beta^{\mathsf{T}} \sigma(\mathsf{W}\mathsf{X} + \mathsf{b})$$

being

- β is a vector of unknown weights
- $\sigma(\cdot)$ is the activation function
- W and b are randomly initialised



Fast boundary reconstruction with PIELM



Given a set of collocation points on the poloidal plane $\{x_i\}_{i=1,...,N}$, the ELM shall satisfy the GS equation at those points

$$\Delta^* \psi_{ELM}(x_i) = \beta^T \Delta^* \sigma(Wx + b) = 0$$

which is equivalent to

$$\beta^T D_{\psi} = 0$$

being D_{ψ} a matrix that can be computed offline.

By exploiting similar argument the ELM can be linked to the poloidal magnetic field measures

$$\beta^T D_B = m_B$$

Fast boundary reconstruction with PIELM



■ PIELM can be trained to satisfy the GS equation and magnetic measurements by minizimizing the cost function

$$Loss(\beta) = \|\beta^{T} D_{\psi}\| + \|\beta^{T} \sigma(W x_{\psi} + b) - m_{\psi}\| + \|\beta^{T} D_{B} - m_{B}\|$$

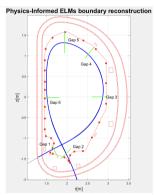
- Hence, standard least-squares methods are sufficient to train the ELM weights (pseudo-inverse) ⇒ PIELM can be trained in real-time!
- If $\beta = E\tilde{\beta}$, with $D_{\psi}^T E = 0$, then it is always $\|\beta^T D_{\psi}\| = 0$ ⇒ the PIELM satisfies the GS equation by design and the weights are trained only to fit the measures

Preliminary results on DTT



- This method can train the ELM weights every time a new set of measurements are available
- Once trained, the ELM is not constrained by a grid of points
- Other real-time methods (XLOC, CCS, filamentary reconstruction) need to either identify the boundary locally in several regions or first identify the sources and then put together the contributions

Gap	Error [cm]
1	0.1
2	0.45
3	0.48
4	0.69
5	0.11
6	0.03



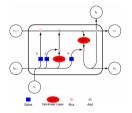
The red dots represent where the solution of the GS equation is set as hard constraint. The blue line is the reconstructed one. The black comes from CREATE-NL

Other possible activities



- Design an LSTM estimator for eddy-currents, instead Kalman filters based on linear models
- Design of adaptive and robust magnetic control components, such as a Model-Reference Adaptive Control (MRAC) for Vertical Stabilization
- Surrogate data-driven model to speed up nonlinear simulations
- Data-driven model for gyrotrons control (Andrea Antonione ECRH group)

. . .



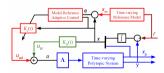




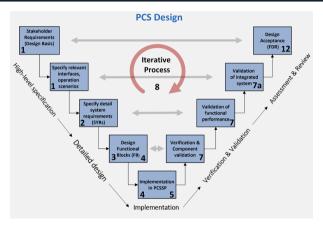
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V-cycle – The ITER *flavour*







P. de Vries et al.

Strategy to systematically design and deploy the ITER plasma control system: A system engineering and model-based design approach Fus. Eng. Des., 2024

LLM support for System-Engineering – 1/2



What's goin' on...



J. J. Norheim et al.

Challenges in applying large language models to requirements engineering tasks Design Science. 2024

- Requirements Engineering
 - Assist in drafting, clarifying, and validating system requirements (i.e., make them testable)
 - Detect ambiguities, inconsistencies (e.g., between SHRs and SYRs), or missing elements in requirement documents
- Model-Based Systems Engineering
 - Translate natural-language requirements into SysML/UML elements
 - Generate system diagrams or design artifacts from textual descriptions

LLM support for System-Engineering – 2/2



- System Architecture & Design Support
 - Propose alternative architectures based on constraints and objectives
- Simulation & Testing
 - Generate test cases/scenarios from requirements
 - Automate setup assessments (in PCSSP, at least for atomic ones)
- Risk & Safety Analysis
 - Help identify potential hazards or failure modes from design documents



Previous Experience & Proposal for Future Work

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Plasma Control ISFN Meeting - ITER HQ, 23 Sep 2025

