

$$\overset{\text{W}}{\text{W}} := 1200 \text{ kgf} \quad X_{cg} := 0.3 \cdot \text{Cma} \quad CD0 := 0.03 \quad \text{etot} := 0.8 \quad \rho := 1.225 \frac{\text{kg}}{\text{m}^3}$$

ALA

$$\begin{aligned} b &:= 10 \text{ m} & Cr &:= 1.6 \text{ m} & \lambda &:= 0.5 & \varepsilon_r &:= 0 \text{ deg} & \varepsilon_t &:= -3 \text{ deg} \\ \alpha_{0L2dwt} &:= -2.5 \text{ deg} & \alpha_{0L2dwr} &:= -1.5 \text{ deg} & iw &:= 2 \text{ deg} & CL\alpha_{2d} &:= 0.11 \text{ deg}^{-1} \\ C_{m_{acw3D}} &:= -0.08 & X_{acw} &:= 0.25 \cdot \text{Cma} & ew &:= 0.9 \\ \eta_i &:= 0.7 & \eta_f &:= 1 & \tau_{alett} &:= 0.40 & \overset{\text{Gamma}}{\Gamma} &:= 5 \text{ deg} \end{aligned}$$

FUSOLIERA

$$C_{m0_f} := -0.05 \quad C_{m\alpha_f} := 0.0035 \text{ deg}^{-1} \quad C_{N\beta_f} := -0.0035 \text{ deg}^{-1}$$

PIANO ORIZZONTALE

$$CL\alpha_{2d} := 0.11 \text{ deg}^{-1} \quad bh := 3.5 \text{ m} \quad Sh := 3 \text{ m}^2 \quad ARh := \frac{bh^2}{Sh} \quad ARh = 4.083$$

$$eh := 0.9$$

$$\eta_h := 1 \quad \tau_e := 0.40 \quad ih := -2 \text{ deg} \quad X_{ach} := 4 \text{ m} \quad Ch\alpha := -0.0080 \text{ deg}^{-1}$$

$$Ch\delta_e := -0.013 \text{ deg}^{-1}$$

PIANO VERTICALE

$$\overset{S_v}{S_v} := 4.5 \text{ m}^2 \quad lv := 5 \text{ m} \quad CL\alpha_{3Dv} := 0.0525 \text{ deg}^{-1} \quad CL\alpha_{3Dv} = 3.008$$

$$\tau_r := 0.50 \quad d\sigma d\beta := 0.11 \quad hv := 1.6 \text{ m} \quad \eta_v := 1$$

$$\overset{V}{V} := 150 \frac{\text{km}}{\text{hr}}$$

SOLUZIONE

$$C_{ma} := \frac{2 \cdot (\lambda^2 + \lambda + 1) \cdot Cr}{3(\lambda + 1)} \quad C_{ma} = 1.244 \text{ m} \quad \overset{S}{S} := \frac{(Cr + \lambda \cdot Cr) \cdot b}{2} \quad S = 12 \text{ m}^2$$

$$AR := \frac{b^2}{S} \quad AR = 8.333$$

$$bc := Cr \quad Ct := \lambda \cdot Cr \quad ac := \frac{Ct - bc}{\frac{b}{2}} \quad \overset{C(y)}{C(y)} := ac \cdot y + bc$$

$$b\varepsilon := \varepsilon_r \quad a\varepsilon := \frac{\varepsilon_t - b\varepsilon}{\frac{b}{2}} \quad \overset{\varepsilon(y)}{\varepsilon(y)} := a\varepsilon \cdot y + b\varepsilon$$

$$ba := \alpha_{0L2dwr} \quad aa := \frac{\alpha_{0L2dwt} - ba}{\frac{b}{2}} \quad \alpha_{0L2d}(y) := aa \cdot y + ba$$

$$\alpha_{0L3Dw} := \frac{2}{S} \cdot \int_0^{\frac{b}{2}} (\alpha_{0L2d}(y) - \epsilon(y)) \cdot C(y) dy \quad \alpha_{0L3Dw} = -0.611 \cdot \text{deg}$$

$$CL_{\alpha w} := \frac{CL_{\alpha w 2d}}{1 + \frac{CL_{\alpha w 2d}}{\pi \cdot AR \cdot ew}} \quad CL_{\alpha w} = 4.972 \cdot \text{rad}^{-1} \quad CL_{\alpha w} = 0.087 \cdot \text{deg}^{-1}$$

$$ARh := \frac{bh^2}{Sh} \quad ARh = 4.083 \quad CL_{\alpha h} := \frac{CL_{\alpha h 2d}}{1 + \frac{CL_{\alpha h 2d}}{\pi \cdot ARh \cdot eh}} \quad CL_{\alpha h} = 0.071 \cdot \text{deg}^{-1}$$

$$Sh = 3 \text{ m}^2 \quad CL_{\alpha h} = 4.077 \cdot \text{rad}^{-1}$$

$$X_{cg} := 0.3 \cdot C_{ma} \quad X_{acw} := 0.25 \cdot C_{ma} \quad X_{acwb} := X_{acw} - \frac{C_{m\alpha_f}}{CL_{\alpha w}} \cdot C_{ma}$$

$$X_{cg} = 0.373 \text{ m} \quad X_{acw} = 0.311 \text{ m} \quad X_{acwb} = 0.261 \text{ m}$$

Xach è la distanza tra il fuoco dell'ala e quello del piano orizzontale

lh è la distanza tra cg e ac del piano orizzontale

Qui sotto sono tutte grandezze dimensionali

$$lh := X_{ach} - (X_{cg} - X_{acw}) \quad lh = 3.938 \text{ m}$$

Distanze adimensionali per equazione momento:

$$X_{w_ad} := \frac{X_{cg} - X_{acwb}}{C_{ma}} \quad X_{w_ad} = 0.09$$

$$X_{h_ad} := \frac{lh}{C_{ma}} \quad X_{h_ad} = 3.164$$

Troviamo il risultato per comandi liberi (domanda n. 2)

$$d\epsilon d\alpha := \frac{2CL_{\alpha w}}{\pi \cdot AR \cdot ew} \quad d\epsilon d\alpha = 0.422 \quad CL_{0w} := CL_{\alpha w} \cdot (i_w - \alpha_{0L3Dw}) \quad CL_{0w} = 0.227$$

$$\varepsilon_0 := \frac{2CL0_w}{\pi \cdot AR \cdot ew} \quad \varepsilon_0 = 1.102 \cdot \text{deg}$$

$$Cm\alpha := CL\alpha_w \cdot \frac{X_{cg} - X_{acwb}}{Cma} - CL\alpha_h \cdot (1 - d\varepsilon d\alpha) \cdot \left(\frac{lh}{Cma} \cdot \frac{Sh}{S} \cdot \eta h \right) \quad Cm\alpha = -0.025 \cdot \text{deg}^{-1}$$

$$Cm\alpha_{wb} := CL\alpha_w \cdot \frac{X_{cg} - X_{acwb}}{Cma} \quad Cm\alpha_{wb} = 7.839 \times 10^{-3} \cdot \text{deg}^{-1}$$

$$Cm\alpha_t := \left[CL\alpha_h \cdot (1 - d\varepsilon d\alpha) \cdot \left(\frac{lh}{Cma} \cdot \frac{Sh}{S} \cdot \eta h \right) \right] \quad Cm\alpha_t = -0.033 \cdot \text{deg}^{-1}$$

$$F := 1 - \tau_e \cdot \frac{Ch\alpha}{Ch\delta e} \quad F = 0.754$$

$$Cm\alpha_{cl} := CL\alpha_w \cdot \frac{X_{cg} - X_{acwb}}{Cma} - CL\alpha_h \cdot (1 - d\varepsilon d\alpha) \cdot F \cdot \left(\frac{lh}{Cma} \cdot \frac{Sh}{S} \cdot \eta h \right) \quad Cm\alpha_{cl} = -0.017 \cdot \text{deg}^{-1}$$

$$Cm_0 := Cm_{acw3D} + Cm_{0f} + CL0_w \cdot \frac{X_{cg} - X_{acwb}}{Cma} + CL\alpha_h \cdot (\varepsilon_0) \cdot \frac{lh}{Cma} \cdot \frac{Sh}{S} \cdot \eta h \quad Cm_0 = -0.047$$

$$Cm_{ih} := -CL\alpha_h \cdot \left(\frac{lh}{Cma} \cdot \frac{Sh}{S} \cdot \eta h \right) \quad Cm_{ih} = -0.056 \cdot \text{deg}^{-1}$$

$$Cm_{\delta e} := -CL\alpha_h \cdot \left(\frac{lh}{Cma} \cdot \frac{Sh}{S} \cdot \eta h \cdot \tau_e \right) \quad Cm_{\delta e} = -0.023 \cdot \text{deg}^{-1}$$

$$\alpha_t(\alpha) := \alpha - \varepsilon_0 - d\varepsilon d\alpha \cdot \alpha + ih \quad \delta e(\alpha) := \frac{-Ch\alpha \cdot \alpha_t(\alpha)}{Ch\delta e}$$

$$Cm(\alpha) := (Cm_0 + Cm\alpha \cdot \alpha + Cm_{ih} \cdot ih + Cm_{\delta e} \cdot \delta e(\alpha))$$

Qui sotto calcolo la risposta alla domanda n. 2, relativamente all'alfa di equilibrio a comandi liberi e alla corrispondente Velocità di equilibrio, che chiamo Veq. (La variabile V (V=150 Km/h) è invece quella assegnata alla domanda 1 e relativa alla domanda a comandi bloccati)

$$\alpha := 0 \quad \alpha_{eq} := \text{root}(Cm(\alpha), \alpha) \quad \alpha_{eq} = 1.325 \cdot \text{deg} \quad \alpha_t(\alpha) = -3.102 \cdot \text{deg}$$

$$CL_{eq} := CL0_w + CL\alpha_w \cdot \alpha_{eq} \quad CL_{eq} = 0.342 \quad V_{eq} := \sqrt{\frac{2}{\rho} \frac{W}{S} \frac{1}{CL_{eq}}}$$

$$\delta e(\alpha_{eq}) = 1.438 \cdot \text{deg} \quad V_{eq} = 68.464 \frac{m}{s} \quad V_{eq} = 246.471 \cdot \frac{km}{hr}$$

Calcolo PUNTO NEUTRO a comandi bloccati ed a comandi liberi con la formulazione esatta e approssimata

Punto neutro a comandi bloccati approssimato

$$X_N := \frac{X_{acwb}}{C_{ma}} + lh \cdot \frac{Sh}{S \cdot C_{ma}} \cdot \frac{CL_{\alpha h}}{CL_{\alpha w}} \cdot (1 - d\epsilon d\alpha) \quad X_N = 0.585$$

$$X_{N2} := \frac{X_{cg}}{C_{ma}} - \frac{C_{m\alpha}}{CL_{\alpha w}} \quad X_{N2} = 0.585$$

Punto neutro a comandi bloccati esatto (formula con numeratore e denominatore)

$$\text{denom} := 1 + \frac{CL_{\alpha h}}{CL_{\alpha w}} \cdot \frac{Sh \cdot (1 - d\epsilon d\alpha)}{S} \quad \text{denom} = 1.118$$

X_{ach2_ad} è la distanza tra centro aer del PO e riferimento (bordo attacco CMA) adimensionalizzata rispetto alla CMA (vedi trattazione Roskam e file ppt MS_07)

$$X_{ach2_ad} := \frac{(X_{ach} + 0.25C_{ma})}{C_{ma}} \quad X_{ach2_ad} = 3.464$$

$$\text{numer} := \frac{X_{acwb}}{C_{ma}} + \frac{Sh}{S} \cdot \frac{CL_{\alpha h}}{CL_{\alpha w}} \cdot (1 - d\epsilon d\alpha) \cdot X_{ach2_ad} \quad \text{numer} = 0.62$$

$$X_{N_exact} := \frac{\text{numer}}{\text{denom}} \quad X_{N_exact} = 0.554$$

Punto neutro a comandi bloccati esatto (dal Margine statico, conoscendo CM_{α} e CL_{α})

Questo è il CL_{α} dell'intero velivolo

$$CL_{\alpha_tot} := CL_{\alpha w} + CL_{\alpha h} \cdot (1 - d\epsilon d\alpha) \cdot \frac{Sh}{S} \cdot \eta h \quad CL_{\alpha_tot} = 5.562$$

$$X_{N_exact2} := \frac{X_{cg}}{C_{ma}} - \frac{C_{m\alpha}}{CL_{\alpha_tot}} \quad X_{N_exact2} = 0.554$$

PUNTO NEUTRO a comandi liberi

$$F := 1 - \tau_e \cdot \frac{Ch\alpha}{Ch\delta e} \quad F = 0.754$$

Punto neutro com liberi approssimato

$$X_{N_cl} := \frac{X_{acwb}}{C_{ma}} + F \cdot \eta h \cdot \frac{Sh}{S \cdot C_{ma}} \cdot \frac{CL\alpha h}{CL\alpha w} \cdot (1 - d\epsilon d\alpha) \quad X_{N_cl} = 0.492$$

$$X_{N_cl2} := \frac{X_{cg}}{C_{ma}} - \frac{C_{m\alpha_cl}}{CL\alpha w} \quad X_{N_cl2} = 0.492$$

p neutro com liberi esatto

$$CL\alpha_{tot_cl} := CL\alpha w + CL\alpha h \cdot (1 - d\epsilon d\alpha) \cdot \frac{Sh}{S} \cdot \eta h \cdot F \quad CL\alpha_{tot_cl} = 5.417$$

$$X_{N_cl_exact} := \frac{X_{cg}}{C_{ma}} - \frac{C_{m\alpha_cl}}{CL\alpha_{tot_cl}} \quad X_{N_cl_exact} = 0.476$$

Punto neutro a comandi liberi esatto (formula con num e denomin)

$$denom_cl := 1 + \frac{CL\alpha h}{CL\alpha w} \cdot \frac{Sh \cdot (1 - d\epsilon d\alpha) \cdot F}{S} \quad denom_cl = 1.089$$

X_{ach2_ad} è la distanza tra centro aer del PO e riferimento (bordo attacco CMA) adimensionalizzata rispetto alla CMA (vedi trattazione Roskam e file ppt MS_07)

$$X_{ach2_ad} := \frac{(X_{ach} + 0.25C_{ma})}{C_{ma}} \quad X_{ach2_ad} = 3.464$$

$$numer_cl := \frac{X_{acwb}}{C_{ma}} + \frac{Sh}{S} \cdot \frac{CL\alpha h}{CL\alpha w} \cdot (1 - d\epsilon d\alpha) \cdot X_{ach2_ad} \cdot F \quad numer_cl = 0.519$$

$$X_{N_exact_cl} := \frac{numer_cl}{denom_cl} \quad X_{N_exact_cl} = 0.476$$

calcolo potenza comandi liberi (domanda n. 2)

$$CD := CD0 + \frac{CL_{eq}^2}{\pi AR \cdot etot} \quad \underline{T} := \frac{1}{2} \cdot \rho \cdot V_{eq}^2 \cdot S \cdot CD \quad P := T \cdot V$$

$$P = 5.106 \times 10^4 \text{ W}$$

delta e comandi bloccati (domanda n. 1)

$$CL := \frac{W}{\frac{1}{2} \cdot \rho \cdot V^2 \cdot S} \quad CL = 0.922 \quad \underline{\alpha} := \frac{CL - CL_{0w}}{CL_{\alpha w}} \quad \alpha = 8.015 \cdot \text{deg}$$

$$\underline{\delta e} := \frac{-(C_{m0} + C_{m\alpha} \cdot \alpha + C_{mih} \cdot ih)}{C_{m\delta e}} \quad \delta e = -5.899 \cdot \text{deg}$$

$$\alpha_h := \alpha - \epsilon_0 - d\epsilon d\alpha \cdot \alpha + ih + \tau_e \cdot \delta e \quad \alpha_h = -0.83 \cdot \text{deg}$$

$$L_h := 0.5 \cdot V^2 \cdot \rho \cdot CL_{\alpha h} \cdot \alpha_h \cdot S_h \quad \alpha_h = -0.83 \cdot \text{deg} \quad L_h = -19.202 \cdot \text{kgf}$$

$$\underline{CD} := CD0 + \frac{CL^2}{\pi AR \cdot etot} \quad \underline{T} := \frac{1}{2} \cdot \rho \cdot V^2 \cdot S \cdot CD \quad \underline{P} := T \cdot V \quad P = 3.754 \times 10^4 \text{ W}$$

LATERO DIREZIONALE SOLUZIONE (domanda n. 3)

$$V_{lat} := 26 \frac{\text{km}}{\text{hr}} \quad \beta := \text{atan}\left(\frac{V_{lat}}{V}\right) \quad \beta = 9.834 \cdot \text{deg}$$

$$C_N := C_{N\beta} \cdot \beta + C_{N\delta r} \cdot \delta r$$

$$C_{N\beta v} := CL_{\alpha 3Dv} \cdot \frac{l_v}{b} \cdot (1 - d\sigma d\beta) \cdot \eta_v \cdot \frac{S_v}{S} \quad C_{N\beta v} = 0.502 \cdot \text{rad}^{-1} \quad C_{N\beta} := C_{N\beta v} + C_{N\beta f}$$

$$C_{N\beta} = 0.301 \cdot \text{rad}^{-1}$$

$$C_{N\delta r} := -CL_{\alpha 3Dv} \cdot \frac{l_v}{b} \cdot \eta_v \cdot \frac{S_v}{S} \cdot \tau_r \quad C_{N\delta r} = -0.282 \quad \delta r := \frac{-C_{N\beta} \cdot \beta}{C_{N\delta r}} \quad \delta r = 10.511 \cdot \text{deg}$$

$$C_{roll} := C_{roll\beta} \cdot \beta + C_{roll\delta a} \cdot \delta a + C_{roll\delta r} \cdot \delta r$$

$$C_{roll\beta v} := -CL_{\alpha 3Dv} \cdot \frac{h_v}{b} \cdot (1 - d\sigma d\beta) \cdot \eta_v \cdot \frac{S_v}{S} \quad C_{roll\beta v} = -0.161 \cdot \text{rad}^{-1}$$

$$C_{\text{roll}\beta\Gamma} := -2 \cdot \frac{CL\alpha w \cdot \Gamma}{S \cdot b} \cdot \int_0^{\frac{b}{2}} C(y) \cdot y \, dy \quad C_{\text{roll}\beta\Gamma} = -0.096 \cdot \text{rad}^{-1}$$

$$C_{\text{roll}\beta} := C_{\text{roll}\beta v} + C_{\text{roll}\beta\Gamma}$$

$$C_{\text{roll}\delta a} := -2 \cdot \frac{CL\alpha w_{2d} \cdot \tau_{alett}}{S \cdot b} \cdot \int_{\eta_i \cdot \frac{b}{2}}^{\eta_f \cdot \frac{b}{2}} C(y) \cdot y \, dy \quad C_{\text{roll}\delta a} = -0.245$$

$$C_{\text{roll}\delta r} := CL\alpha 3Dv \cdot \frac{h v}{b} \cdot \eta v \cdot \frac{S v}{S} \cdot \tau_r \quad C_{\text{roll}\delta r} = 0.09 \cdot \text{rad}^{-1}$$

$$\delta a := \frac{-C_{\text{roll}\delta r} \cdot \delta r - C_{\text{roll}\beta} \cdot \beta}{C_{\text{roll}\delta a}} \quad \delta a = -6.458 \cdot \text{deg}$$

$$X := \frac{X_{ach}}{C_{ma}} + 0.25 \quad X = 3.464$$

