

## ESAME di Manovre in Volo e Dimensionamento – 14 Gennaio 2009

Sia dato un velivolo con le seguenti caratteristiche:

$W=900 \text{ Kg}$     $CD_0=.03$    e (Fattore di Oswald) = .80   quota=0 m  
 $X_{cg}=30\%$  della corda media aerodinamica

### **Fusoliera:**

$C_{m0f} = -.05$     $C_{m\alpha f} = .0035/\text{grado}$     $C_{n\beta f} = -.35 \cdot 10^{-3}/\text{grado}$

### **Ala trapezia (bordo di attacco dritto):**

$b=10. \text{ m}$     $C_r=1.6 \text{ m}$     $\lambda=.4$     $C_{L\alpha 2D} = .11/\text{grado}$     $X_{acw}=25\% C_{media}$

$\alpha_{0L2Dr} = -1.5 \text{ gradi}$     $\alpha_{0L2Dt} = -2.5 \text{ gradi}$

$C_{Mac3D} = -.08$     $\varepsilon_{tip} = -3^\circ$     $i_w = 3 \text{ gradi}$  rispetto alla retta di costruzione fusoliera

e (Fattore di Oswald) = .9   alettoni:    $\eta_i = .7$     $\eta_f = 1.$     $\tau_{alettoni} = .35$     $\Gamma = 5 \text{ gradi}$

### **Piano orizzontale di coda convenzionale**

$S_H = 3. \text{ m}^2$     $b_H = 2.5 \text{ m}$     $X_{acH} = 4 \text{ m}$     $C_{L\alpha 2DH} = 0.11/\text{grado}$  (profilo simmetrico)

e (Fattore di Oswald) = .9    $\eta_H = 1$    forma in pianta rettangolare

$C_{h\alpha} = -.0080/\text{grado}$     $C_{h\delta e} = -.013/\text{grado}$     $\tau_e = 0.35$     $i_h = -2^\circ$

### **Piano verticale di coda:**

$S_V = 3 \text{ m}^2$     $l_v = 4.5 \text{ m}$     $C_{L\alpha 3DV} = .052/\text{grado}$     $\eta_V = 1$     $h_v = 1 \text{ m}$     $\tau_{timone} = .50$ ;  
 $d\sigma/d\beta = 0.1$

$X_{acH}$  è la distanza tra il centro aerodinamico dell'ala ed il centro aerodinamico del piano orizzontale di coda

$h_v$  e' la distanza verticale media tra il centro aerodinamico del piano di coda e la direzione della velocità'.

Si ipotizzi la portanza totale generata dalla sola ala.

- 1) Calcolare il  $\delta e$  di equilibrio, la posizione del punto neutro, la potenza necessaria ed il carico agente sul piano orizzontale di coda, a comandi bloccati considerando una velocità di volo di 150 km/h.
- 2) Calcolare l'assetto e la velocità necessaria, posizione del punto neutro e potenza necessaria all'equilibrio a comandi liberi.
- 3) Nella stessa situazione del punto 1 si consideri una raffica proveniente dalla destra del pilota con velocità  $V_f = 26 \text{ km/h}$ : calcolare la deflessione del timone e degli alettoni per volare con le ali livellate.

$$\overset{\text{W}}{\text{W}} := 900 \text{ kgf} \quad X_{cg} := 0.3 \cdot C_{ma} \quad CD_0 := 0.03 \quad e_{tot} := 0.8 \quad \rho := 1.225 \frac{\text{kg}}{\text{m}^3}$$

ALA

$$\begin{aligned} b &:= 10 \text{ m} & C_r &:= 1.6 \text{ m} & \lambda &:= 0.4 & \varepsilon_r &:= 0 \text{ deg} & \varepsilon_t &:= -3 \text{ deg} \\ \alpha_{0L2dwt} &:= -2.5 \text{ deg} & \alpha_{0L2dwr} &:= -1.5 \text{ deg} & i_w &:= 3 \text{ deg} & CL_{\alpha w2d} &:= 0.11 \text{ deg}^{-1} \\ C_{m_{acw3D}} &:= -0.08 & X_{acw} &:= 0.25 \cdot C_{ma} & e_w &:= 0.9 \\ \eta_i &:= 0.7 & \eta_f &:= 1 & \tau_{alett} &:= 0.35 & \overset{\text{Gamma}}{\Gamma} &:= 5 \text{ deg} \end{aligned}$$

FUSOLIERA

$$C_{m0_f} := -0.05 \quad C_{m\alpha_f} := 0.0035 \text{ deg}^{-1} \quad C_{N\beta_f} := -0.0035 \text{ deg}^{-1}$$

PIANO ORIZZONTALE

$$\begin{aligned} CL_{\alpha h2d} &:= 0.11 \text{ deg}^{-1} & b_h &:= 2.5 \text{ m} & S_h &:= 2.5 \text{ m}^2 & e_h &:= 0.9 \\ \eta_h &:= 1 & \tau_e &:= 0.35 & i_h &:= -2 \text{ deg} & X_{ach} &:= 4 \text{ m} & Ch_{\alpha} &:= -0.0080 \text{ deg}^{-1} \\ & & & & & & Ch_{\delta e} &:= -0.013 \text{ deg}^{-1} \end{aligned}$$

PIANO VERTICALE

$$\begin{aligned} \overset{S_v}{S_v} &:= 3 \text{ m}^2 & l_v &:= 4.5 \text{ m} & CL_{\alpha 3Dv} &:= 0.052 \text{ deg}^{-1} & \eta_v &:= 1 \\ \tau_r &:= 0.5 & d\sigma d\beta &:= 0.1 & h_v &:= 1 \text{ m} \end{aligned}$$

$$\overset{V}{V} := 150 \frac{\text{km}}{\text{hr}}$$

SOLUZIONE

$$C_{ma} := \frac{2 \cdot (\lambda^2 + \lambda + 1) \cdot C_r}{3(\lambda + 1)} \quad C_{ma} = 1.189 \text{ m} \quad \overset{S}{S} := \frac{(C_r + \lambda \cdot C_r) \cdot b}{2} \quad S = 11.2 \text{ m}^2$$

$$AR := \frac{b^2}{S} \quad AR = 8.929$$

$$\begin{aligned} bc &:= C_r & Ct &:= \lambda \cdot C_r & ac &:= \frac{Ct - bc}{\frac{b}{2}} & \overset{C}{C}(y) &:= ac \cdot y + bc \\ b\varepsilon &:= \varepsilon_r & a\varepsilon &:= \frac{\varepsilon_t - b\varepsilon}{\frac{b}{2}} & \overset{\varepsilon}{\varepsilon}(y) &:= a\varepsilon \cdot y + b\varepsilon \end{aligned}$$

$$ba := \alpha_{0L2dwr} \quad aa := \frac{\alpha_{0L2dwt} - ba}{\frac{b}{2}} \quad \alpha_{0L2d}(y) := aa \cdot y + ba$$

$$\alpha_{0L3Dw} := \frac{2}{S} \cdot \int_0^{\frac{b}{2}} (\alpha_{0L2d}(y) - \varepsilon(y)) \cdot C(y) dy \quad \alpha_{0L3Dw} = -0.643 \text{ deg}$$

$$CL_{\alpha w} := \frac{CL_{\alpha w 2d}}{1 + \frac{CL_{\alpha w 2d}}{\pi \cdot AR \cdot ew}} \quad CL_{\alpha w} = 5.043 \text{ rad}^{-1} \quad CL_{\alpha w} = 0.088 \text{ deg}^{-1}$$

$$AR_h := \frac{bh^2}{Sh} \quad AR_h = 2.5 \quad CL_{\alpha h} := \frac{CL_{\alpha h 2d}}{1 + \frac{CL_{\alpha h 2d}}{\pi \cdot AR_h \cdot eh}} \quad CL_{\alpha h} = 0.058 \text{ deg}^{-1}$$

$$Sh = 2.5 \text{ m}^2 \quad CL_{\alpha h} = 3.332 \text{ rad}^{-1}$$

$$X_{cg} := 0.3 \cdot C_{ma} \quad X_{acw} := 0.25 \cdot C_{ma} \quad X_{acwb} := X_{acw} - \frac{C_{m\alpha_f}}{CL_{\alpha w}} \cdot C_{ma}$$

$$X_{cg} = 0.357 \text{ m} \quad X_{acw} = 0.297 \text{ m} \quad X_{acwb} = 0.25 \text{ m}$$

Xach è la distanza tra il fuoco dell'ala e quello del piano orizzontale

lh è la distanza tra cg e ac del piano orizzontale

Qui sotto sono tutte grandezze dimensionali

$$lh := X_{ach} - (X_{cg} - X_{acw}) \quad lh = 3.941 \text{ m}$$

Distanze adimensionali per equazione momento:

$$X_{w\_ad} := \frac{X_{cg} - X_{acwb}}{C_{ma}} \quad X_{w\_ad} = 0.09$$

$$X_{h\_ad} := \frac{lh}{C_{ma}} \quad X_{h\_ad} = 3.315$$

Troviamo il risultato  
per comandi liberi

$$d\varepsilon d\alpha := \frac{2CL_{\alpha w}}{\pi \cdot AR \cdot ew} \quad d\varepsilon d\alpha = 0.4 \quad CL_{0w} := CL_{\alpha w} \cdot (i_w - \alpha_{0L3Dw}) \quad CL_{0w} = 0.321$$

$$\varepsilon_0 := \frac{2CL_{0w}}{\pi \cdot AR \cdot ew} \quad \varepsilon_0 = 1.456 \text{ deg}$$

$$C_{m\alpha} := CL_{\alpha w} \cdot \frac{X_{cg} - X_{acwb}}{C_{ma}} - CL_{\alpha h} \cdot (1 - d\varepsilon d\alpha) \cdot \left( \frac{lh}{C_{ma}} \cdot \frac{Sh}{S} \cdot \eta h \right) \quad C_{m\alpha} = -0.018 \text{ deg}^{-1}$$

$$Cm\alpha_{wb} := CL\alpha_w \cdot \frac{X_{cg} - X_{acwb}}{Cma} \quad Cm\alpha_{wb} = 7.901 \times 10^{-3} \text{ deg}^{-1}$$

$$Cm\alpha_t := \left[ CL\alpha_h \cdot (1 - d\epsilon d\alpha) \cdot \left( \frac{lh}{Cma} \cdot \frac{Sh}{S} \cdot \eta h \right) \right] \quad Cm\alpha_t = -0.026 \text{ deg}^{-1}$$

$$F := 1 - \tau_e \cdot \frac{Ch\alpha}{Ch\delta e} \quad F = 0.785$$

$$Cm\alpha_{cl} := CL\alpha_w \cdot \frac{X_{cg} - X_{acwb}}{Cma} - CL\alpha_h \cdot (1 - d\epsilon d\alpha) \cdot F \cdot \left( \frac{lh}{Cma} \cdot \frac{Sh}{S} \cdot \eta h \right) \quad Cm\alpha_{cl} = -0.012 \text{ deg}^{-1}$$

$$Cm0 := Cm_{acw3D} + Cm0_f + CL0_w \cdot \frac{X_{cg} - X_{acwb}}{Cma} + CL\alpha_h \cdot (\epsilon0) \cdot \frac{lh}{Cma} \cdot \frac{Sh}{S} \cdot \eta \quad Cm0 = -0.039$$

$$Cmih := -CL\alpha_h \cdot \left( \frac{lh}{Cma} \cdot \frac{Sh}{S} \cdot \eta h \right) \quad Cmih = -0.043 \text{ deg}^{-1}$$

$$Cm\delta e := -CL\alpha_h \cdot \left( \frac{lh}{Cma} \cdot \frac{Sh}{S} \cdot \eta h \cdot \tau_e \right) \quad Cm\delta e = -0.015 \text{ deg}^{-1}$$

$$\alpha_t(\alpha) := \alpha - \epsilon0 - d\epsilon d\alpha \cdot \alpha + ih \quad \delta e(\alpha) := \frac{-Ch\alpha \cdot \alpha_t(\alpha)}{Ch\delta e}$$

$$Cm(\alpha) := (Cm0 + Cm\alpha \cdot \alpha + Cmih \cdot ih + Cm\delta e \cdot \delta e(\alpha))$$

$$\alpha := 0 \quad \alpha_{eq} := \text{root}(Cm(\alpha), \alpha) \quad \alpha_{eq} = 1.25 \text{ deg} \quad \alpha_t(\alpha) = -3.456 \text{ deg}$$

$$CL_{eq} := CL0_w + CL\alpha_w \cdot \alpha_{eq} \quad CL_{eq} = 0.431 \quad V_{eq} := \sqrt{\frac{2}{\rho} \frac{W}{S} \frac{1}{CL_{eq}}} \quad V_{eq} = 54.659 \frac{m}{s}$$

$$\delta e(\alpha_{eq}) = 1.665 \text{ deg} \quad V_{eq} = 196.771 \frac{kn}{hr}$$

$$F := 1 - \tau_e \cdot \frac{Ch\alpha}{Ch\delta e} \quad X_{N_{cl}} := \frac{X_{acwb}}{Cma} + F \cdot lh \cdot \frac{Sh}{S \cdot Cma} \cdot \frac{CL\alpha_h}{CL\alpha_w} \cdot (1 - d\epsilon d\alpha) \quad X_{N_{cl}} = 0.441$$

$$X_{N_{cl2}} := \frac{X_{cg}}{Cma} - \frac{Cm\alpha_{cl}}{CL\alpha_w} \quad X_{N_{cl2}} = 0.441$$

Punto neutro a comandi bloccati approssimato

$$X_N := \frac{X_{acwb}}{Cma} + lh \cdot \frac{Sh}{S \cdot Cma} \cdot \frac{CL\alpha_h}{CL\alpha_w} \cdot (1 - d\epsilon d\alpha) \quad X_N = 0.504$$

$$X_{N2} := \frac{X_{cg}}{C_{ma}} - \frac{C_{m\alpha}}{CL_{\alpha w}} \quad X_{N2} = 0.504$$

Punto neutro a comandi bloccati esatto

$$\text{denom} := 1 + \frac{CL_{\alpha h}}{CL_{\alpha w}} \cdot \frac{Sh \cdot (1 - d\epsilon d\alpha)}{S} \quad \text{denom} = 1.089$$

$X_{ach2\_ad}$  è la distanza tra centro aer del PO e riferimento (bordo attacco CMA) adimensionalizzata rispetto alla CMA (vedi trattazione Roskam e file ppt MS\_07)

$$X_{ach2\_ad} := \frac{(X_{ach} + 0.25C_{ma})}{C_{ma}} \quad X_{ach2\_ad} = 3.615$$

$$\text{numer} := \frac{X_{acwb}}{C_{ma}} + \frac{Sh}{S} \cdot \frac{CL_{\alpha h}}{CL_{\alpha w}} \cdot (1 - d\epsilon d\alpha) \cdot X_{ach2\_ad} \quad \text{numer} = 0.53$$

$$X_{N\_exact} := \frac{\text{numer}}{\text{denom}} \quad X_{N\_exact} = 0.487$$

$$CL_{\alpha\_tot} := CL_{\alpha w} + CL_{\alpha h} \cdot (1 - d\epsilon d\alpha) \cdot \frac{Sh}{S} \cdot \eta h \quad CL_{\alpha\_tot} = 5.49$$

$$X_{N\_exact2} := \frac{X_{cg}}{C_{ma}} - \frac{C_{m\alpha}}{CL_{\alpha\_tot}} \quad X_{N\_exact2} = 0.487$$

calcolo potenza comandi liberi

$$CD := CD_0 + \frac{CL_{eq}^2}{\pi AR \cdot \epsilon_{tot}} \quad T_{\text{res}} := \frac{1}{2} \cdot \rho \cdot V_{eq}^2 \cdot S \cdot CD \quad P := T \cdot V$$

$$P = 3.268 \times 10^4 \text{ W}$$

delta e comandi bloccati

$$CL := \frac{W}{\frac{1}{2} \cdot \rho \cdot V^2 \cdot S} \quad CL = 0.741 \quad \alpha_{\text{res}} := \frac{CL - CL_{0w}}{CL_{\alpha w}} \quad \alpha = 4.776 \text{ deg}$$

$$\delta e_{\text{res}} := \frac{-(C_{m0} + C_{m\alpha} \cdot \alpha + C_{mih} \cdot ih)}{C_{m\delta e}} \quad \delta e = -2.535 \text{ deg}$$

$$X_N := \frac{X_{cg}}{C_{ma}} - \frac{C_{m\alpha}}{CL_{\alpha w}} \quad X_N = 0.504 \quad \alpha_h := \alpha - \epsilon_0 - d\epsilon d\alpha \cdot \alpha + ih + \tau_e \cdot \delta e \quad \alpha_h = -1.475 \text{ deg}$$

$$L_h := 0.5 \cdot V^2 \cdot \rho \cdot CL_{\alpha h} \cdot \alpha_h \cdot S_h \quad \alpha_h = -1.475 \text{ deg} \quad L_h = -23.253 \text{ kgf}$$

$$\underline{C_D} := CD_0 + \frac{CL^2}{\pi AR \cdot \text{etot}} \quad \underline{T} := \frac{1}{2} \cdot \rho \cdot V^2 \cdot S \cdot CD \quad \underline{P} := T \cdot V \quad P = 2.703 \times 10^4 \text{ W}$$

LATERO DIREZIONALE  
SOLUZIONE

$$V_{lat} := 26 \frac{\text{km}}{\text{hr}} \quad \beta := \text{atan}\left(\frac{V_{lat}}{V}\right) \quad \beta = 9.834 \text{ deg}$$

$$C_N := C_{N\beta} \cdot \beta + C_{N\delta r} \cdot \delta_r$$

$$C_{N\beta v} := CL\alpha_3 Dv \cdot \frac{l_v}{b} \cdot (1 - d\sigma d\beta) \cdot \eta_v \cdot \frac{S_v}{S} \quad C_{N\beta v} = 0.323 \text{ rad}^{-1} \quad C_{N\beta} := C_{N\beta v} + C_{N\beta f}$$

$$C_{N\beta} = 0.123 \text{ rad}^{-1}$$

$$C_{N\delta r} := -CL\alpha_3 Dv \cdot \frac{l_v}{b} \cdot \eta_v \cdot \frac{S_v}{S} \cdot \tau_r \quad C_{N\delta r} = -0.18 \quad \delta_r := \frac{-C_{N\beta} \cdot \beta}{C_{N\delta r}} \quad \delta_r = 6.718 \text{ deg}$$

$$C_{roll} := C_{roll\beta} \cdot \beta + C_{roll\delta a} \cdot \delta a + C_{roll\delta r} \cdot \delta r$$

$$C_{roll\beta v} := -CL\alpha_3 Dv \cdot \frac{h_v}{b} \cdot (1 - d\sigma d\beta) \cdot \eta_v \cdot \frac{S_v}{S} \quad C_{roll\beta v} = -0.072 \text{ rad}^{-1}$$

$$C_{roll\beta\Gamma} := -2 \cdot \frac{CL\alpha_w 2d \cdot \Gamma}{S \cdot b} \cdot \int_0^{\frac{b}{2}} C(y) \cdot y \, dy \quad C_{roll\beta\Gamma} = -0.118 \text{ rad}^{-1}$$

$$C_{roll\beta} := C_{roll\beta v} + C_{roll\beta\Gamma}$$

$$C_{roll\delta a} := -2 \cdot \frac{CL\alpha_w 2d \cdot \tau_{alett}}{S \cdot b} \cdot \int_{\eta_i \cdot \frac{b}{2}}^{\eta_f \cdot \frac{b}{2}} C(y) \cdot y \, dy$$

$$C_{roll\delta a} = -0.195$$

$$C_{roll\delta r} := CL\alpha_3 Dv \cdot \frac{h_v}{b} \cdot \eta_v \cdot \frac{S_v}{S} \cdot \tau_r \quad C_{roll\delta r} = 0.04 \text{ rad}^{-1}$$

$$\delta a := \frac{-C_{\text{roll}\delta r} \cdot \delta r - C_{\text{roll}\beta} \cdot \beta}{C_{\text{roll}\delta a}} \quad \delta a = -8.201 \text{ deg}$$

$$X := \frac{X_{ach}}{C_{ma}} + 0.25 \quad X = 3.615$$





